

### TYPICAL TUNNEL LINING SECTION DEMENSION IN MM





PROJECT







National Highways and Infrastructure Development Corporation PTI Bullding ,4 Parliament Street, Sansad Marg Area, New Delhi,Delhi 110001

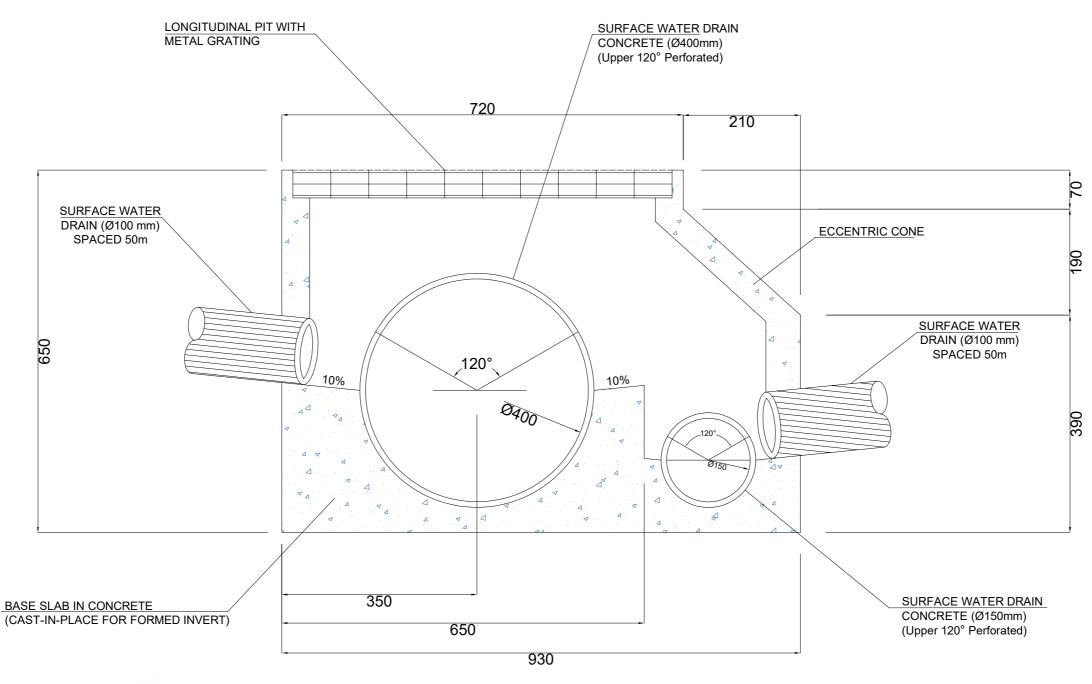
Construction Of Bi Directional tunnel at km 83 of length 495m Including approaches road of 664 m and a major bridge of 110 m from km 82 +675 to km 82 +925 on NH- 244







DRAWN BY: CARMEN PEREZ SERRANO TUNNEL DRAINAGE SYSTEM TYPICAL CROSS SECTION DESIGNED BY : DIANA CASTANEDO DE LUCAS CHECKED BY: PROF.FCO.CASTENEDO NAVARRO RECOMMENDED BY : DIANA CASTANEDO LUCAS KDBT/DREIN/IND/R1 APPROVED BY: PROF.FCO.CASTENEDO NAVARRO R1









DIMENSIONS IN mm

DESIGN CONSULTANT

CLIENT



National Highways and Infrastructure Development Corporation

PTI Bullding ,4 Parliament Street, Sansad Marg Area, New Delhi, Delhi 110001

PROJECT

Construction Of Bi Directional tunnel at km 83 of length 495m Including approaches road of 664 m and a major bridge of 110 m from km 82 +675 to km 82 +925 on NH- 244



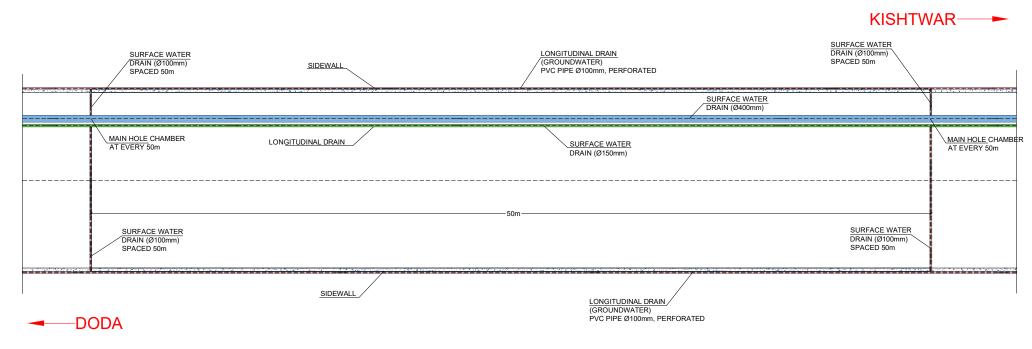
SECL Space Engineers Consortium Pvt.Ltd In associated with Equipo De Prospecciones ,S.A

SA

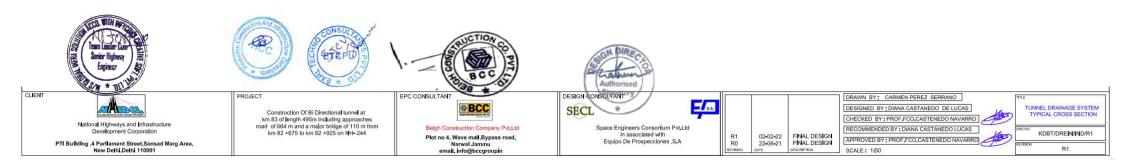
02-02-22 22-06-21 FINAL DESIGN FINAL DESIGN

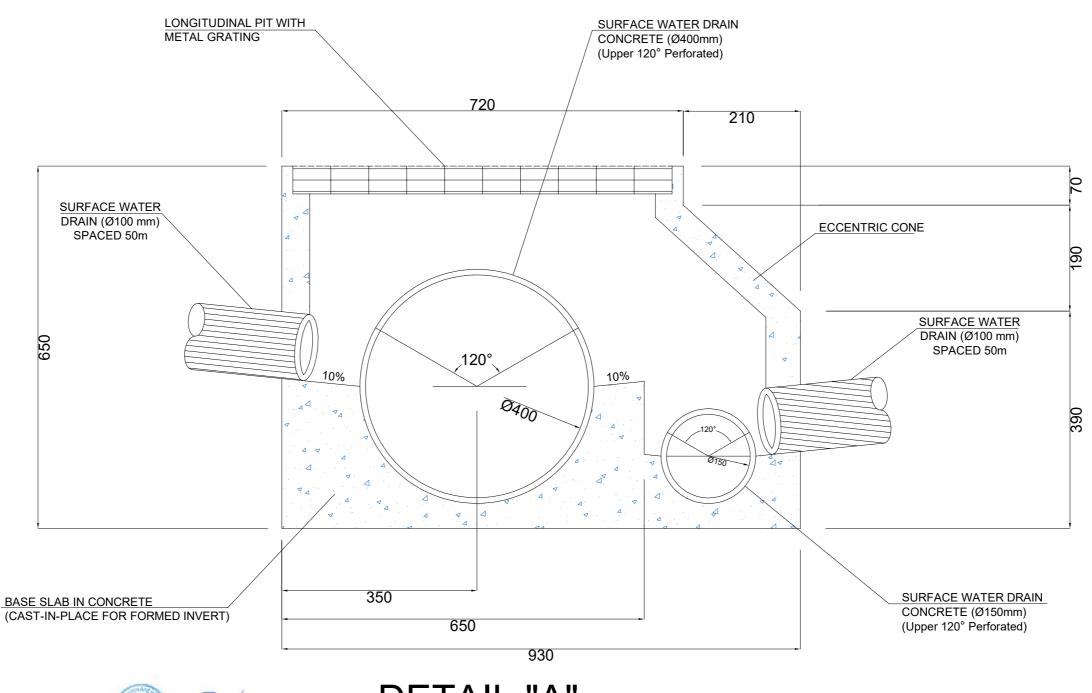
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TUNNEL DRAINAGE SYSTEM TYPICAL CROSS SECTION KDBT/DREIN/IND/R1



#### **DETAIL PLAN**



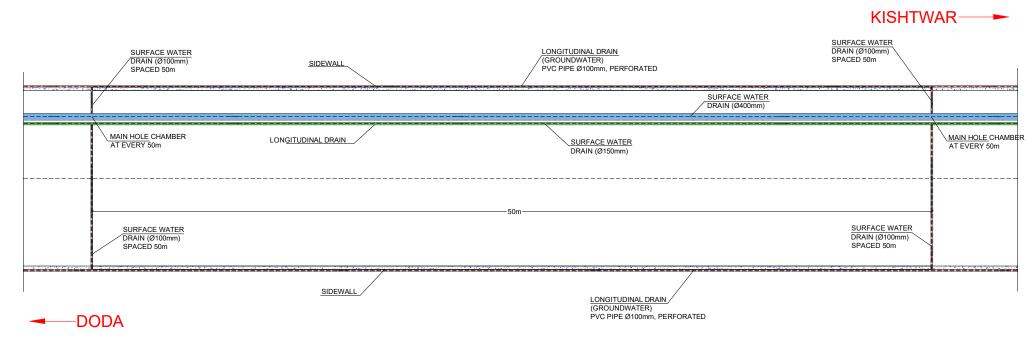






## DETAIL "A"

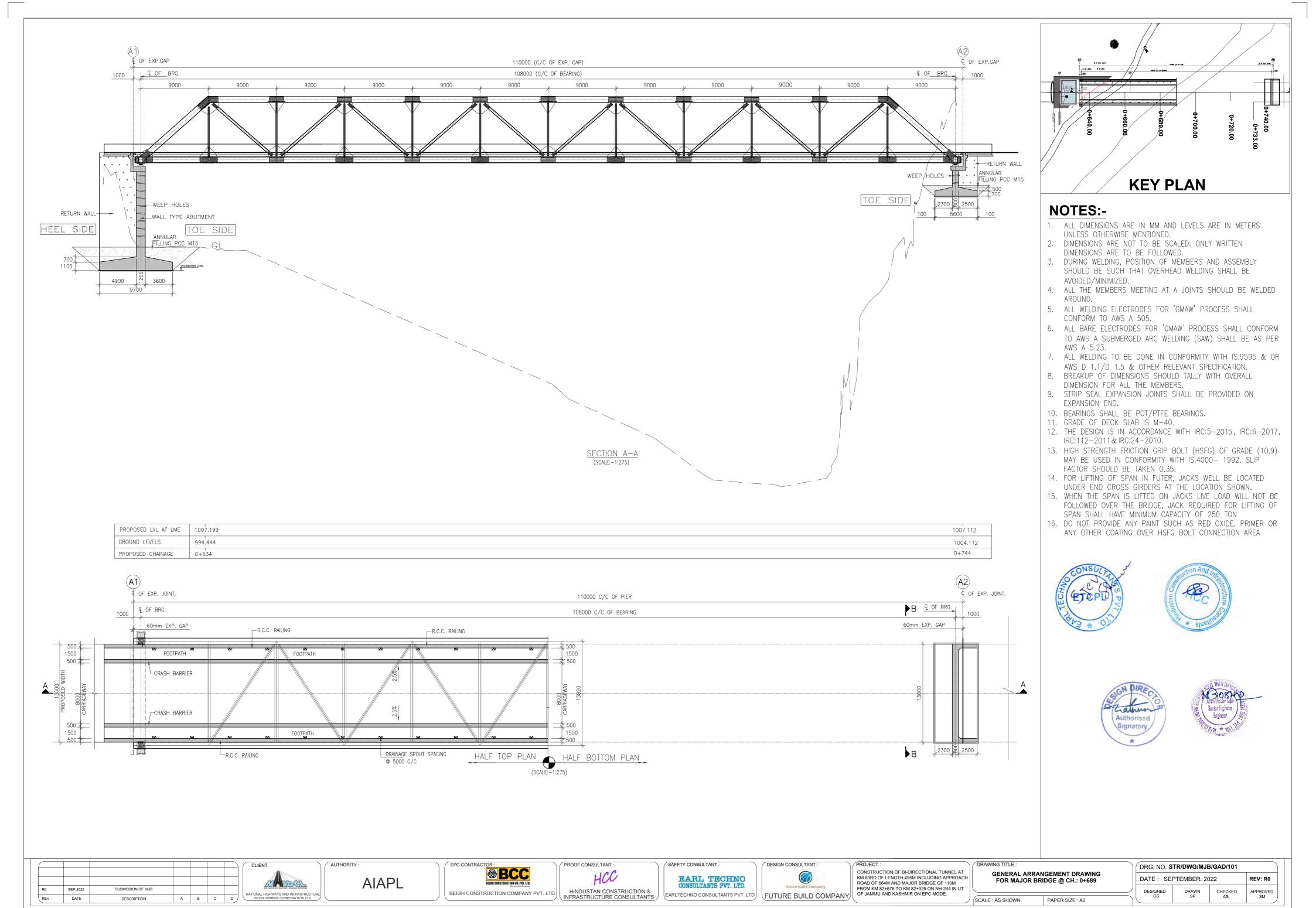
EPC CONSULTANT DESIGN CONSULTANT DRAWN BY: CARMEN PEREZ SERRANO SA TUNNEL DRAINAGE SYSTEM TYPICAL CROSS SECTION BCC DESIGNED BY: DIANA CASTANEDO DE LUCAS Construction Of Bi Directional tunnel at km 83 of length 495m Including approaches road of 664 m and a major bridge of 110 m from km 82 +675 to km 82 +925 on NH- 244 SECL CHECKED BY: PROF.FCO.CASTENEDO NAVARRO National Highways and Infrastructure Space Engineers Consortium Pvt.Ltd In associated with Equipo De Prospecciones ,S.A RECOMMENDED BY : DIANA CASTANEDO LUCAS KDBT/DREIN/IND/R1 02-02-22 22-06-21 FINAL DESIGN FINAL DESIGN Plot no 4, Wave mall, Bypass road, APPROVED BY : PROF.FCO.CASTENEDO NAVARRO PTI Bullding ,4 Parliament Street, Sansad Marg Area, New Delhi, Delhi 110001 Narwal Jammu email. info@bccgroupi

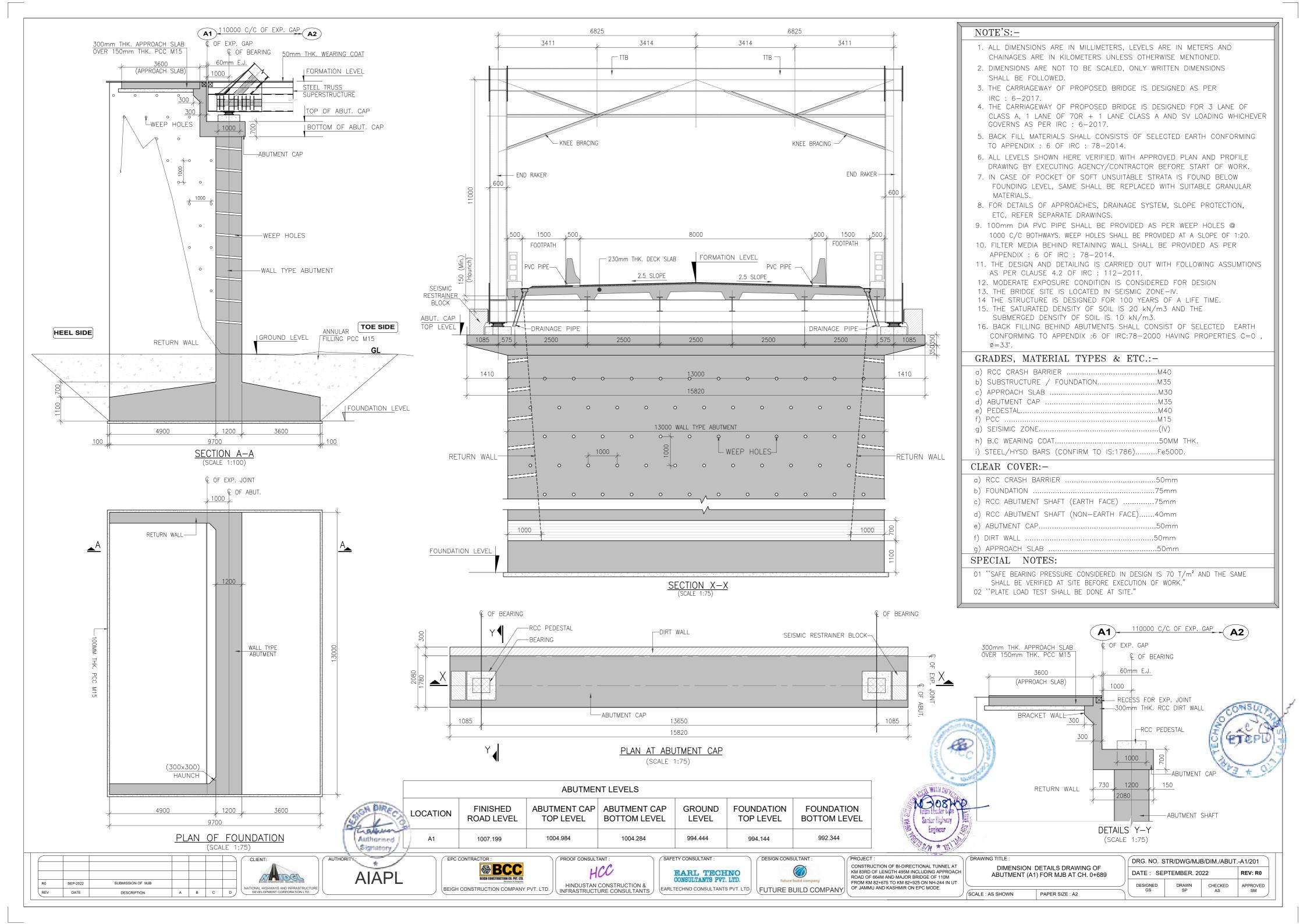


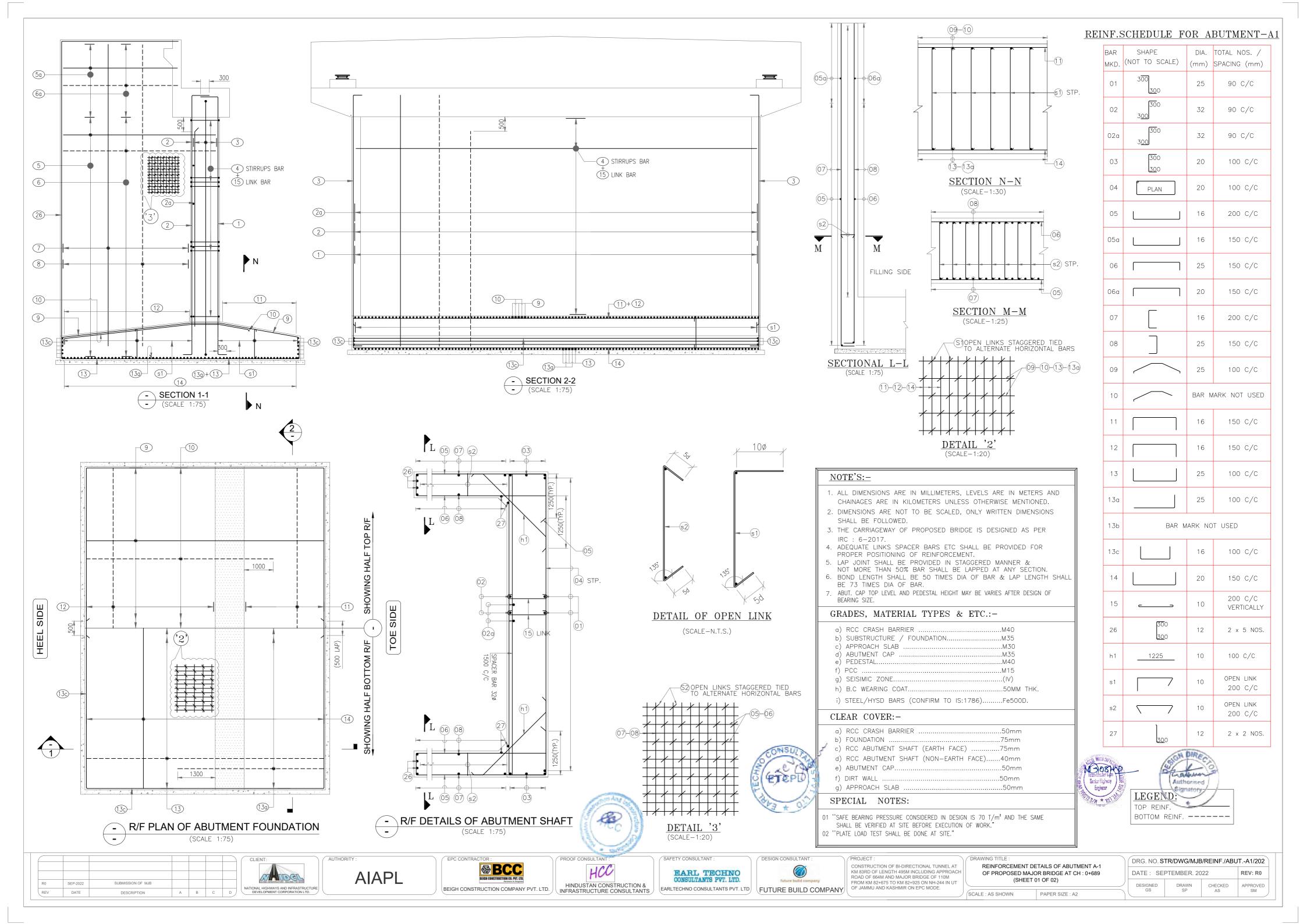
### **DETAIL PLAN**

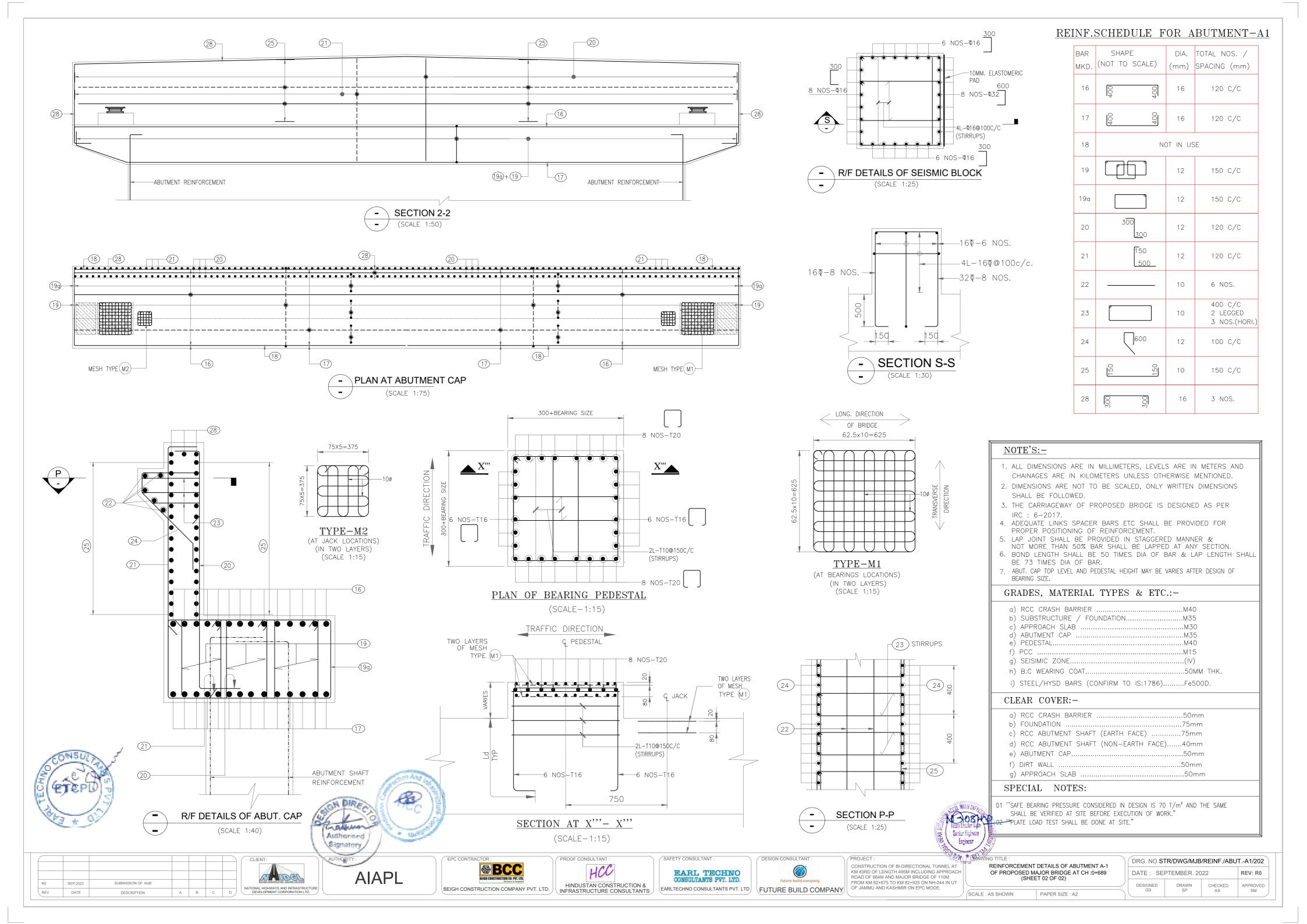


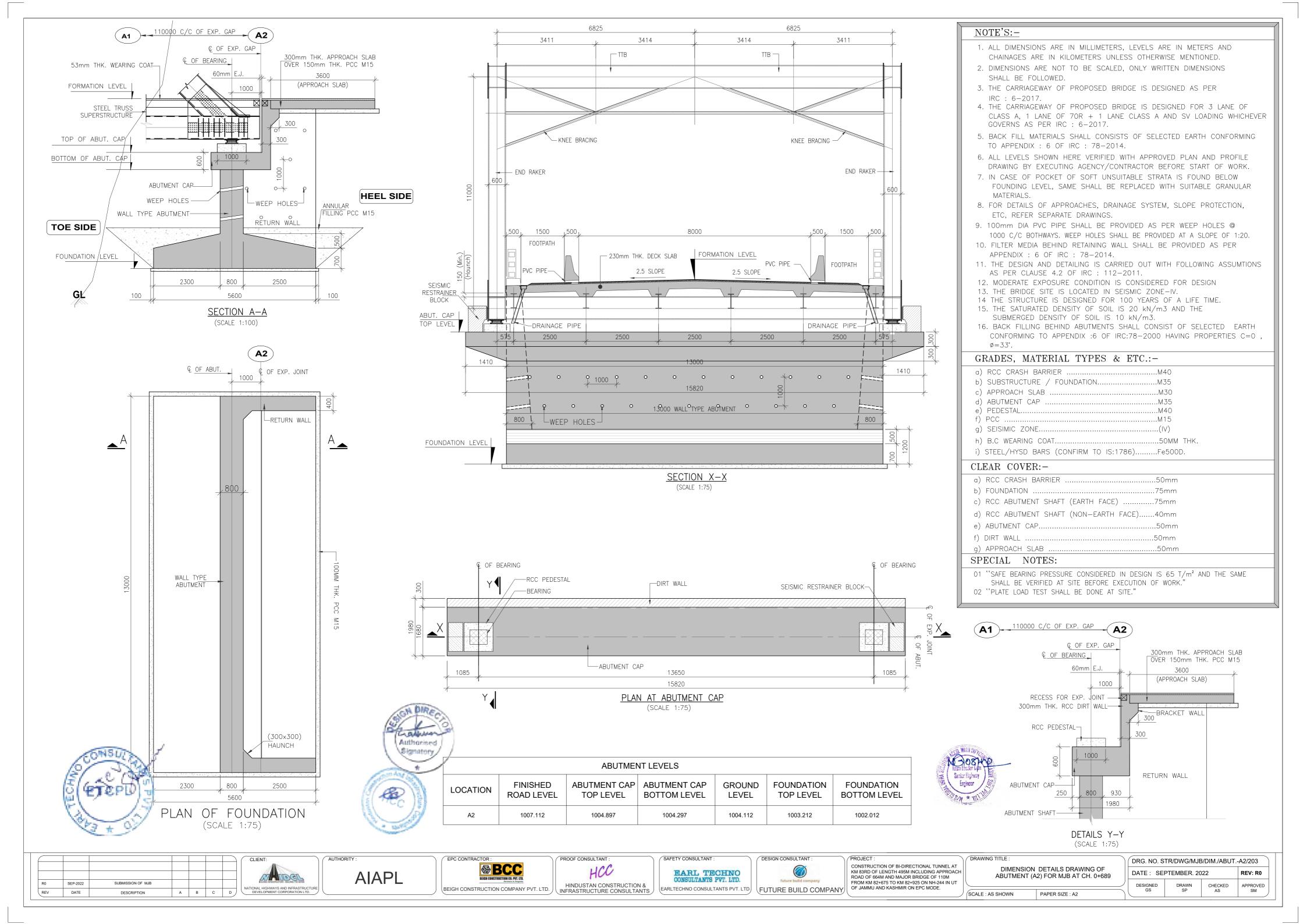


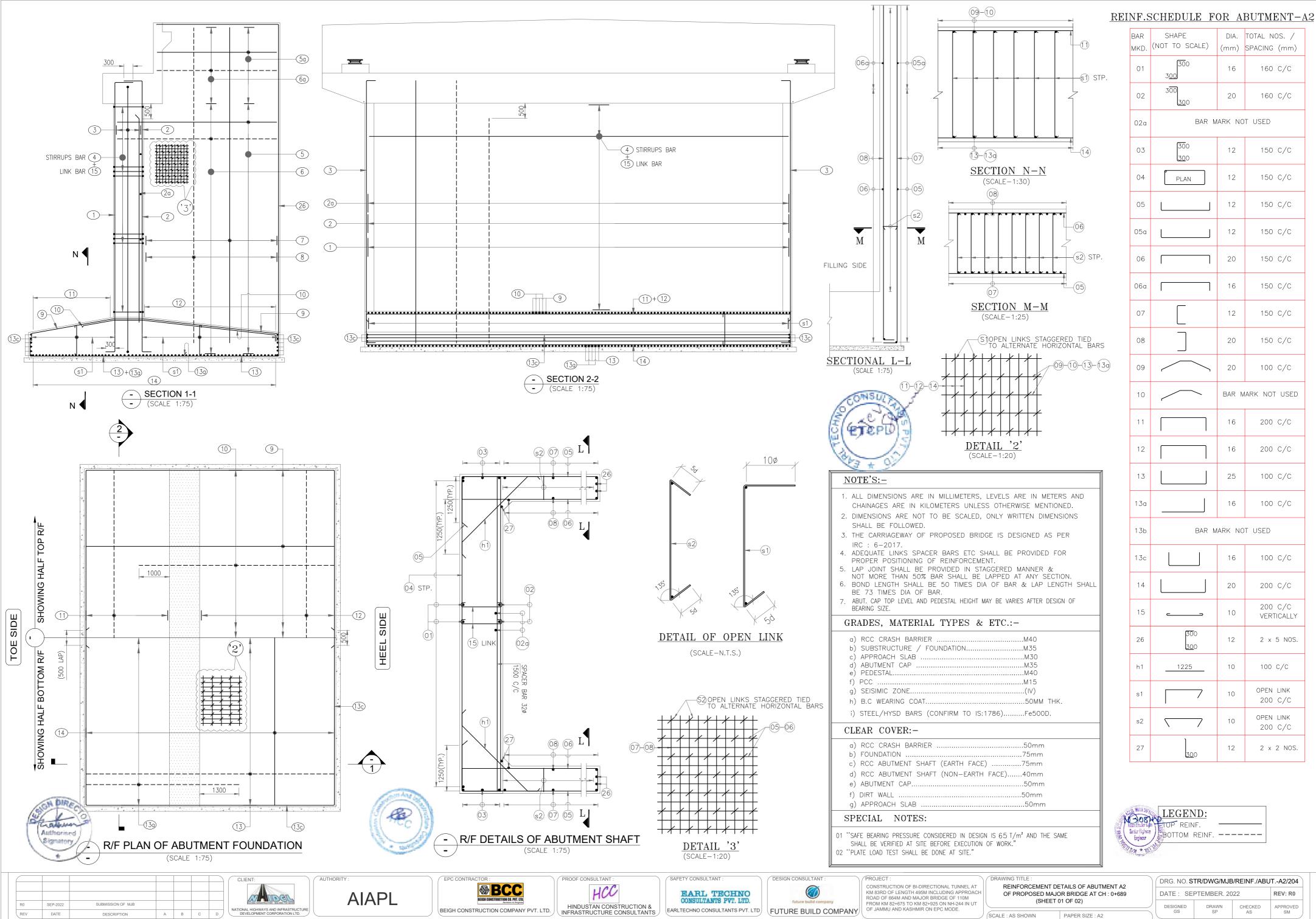












DIA. TOTAL NOS. / (mm) SPACING (mm) 160 C/C 160 C/C 20 BAR MARK NOT USED 12 150 C/C 150 C/C 150 C/C 150 C/C 150 C/C 150 C/C 12 150 C/C 20 150 C/C 100 C/C BAR MARK NOT USED 200 C/C 200 C/C 100 C/C 25 100 C/C BAR MARK NOT USED 100 C/C 200 C/C 200 C/C 10 VERTICALLY 2 x 5 NOS.



DRG. NO. STR/DWG/MJB/REINF./ABUT.-A2/204 DATE: SEPTEMBER. 2022 CHECKED AS APPROVED SM

100 C/C

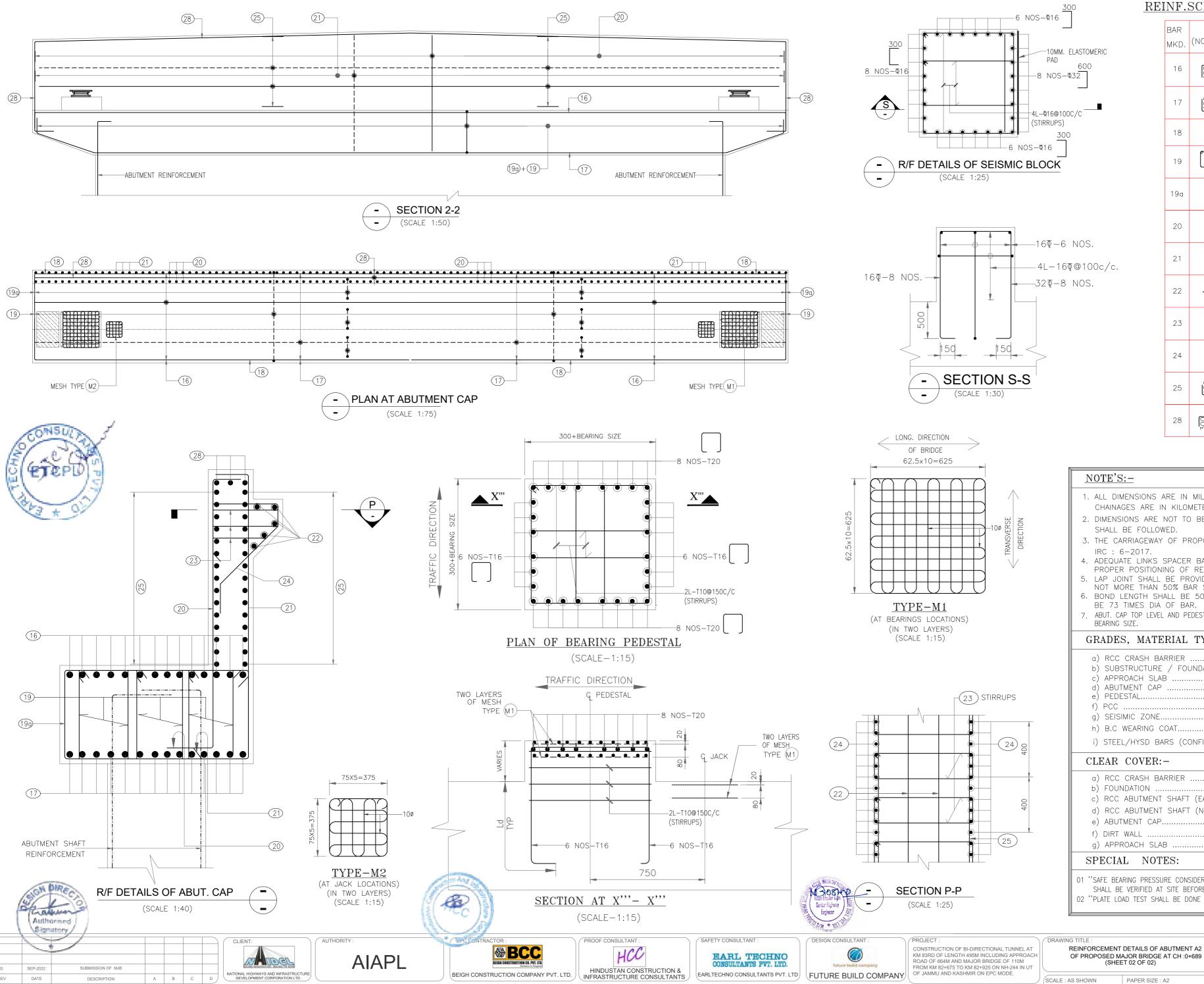
OPEN LINK

200 C/C

OPEN LINK

200 C/C

2 x 2 NOS.



### REINF.SCHEDULE FOR ABUTMENT-A2

BAR MKD. (NOT TO SCALE) DIA. TOTAL NOS. / (mm) SPACING (mm)  16	NF.	SCHEDULE F	OR A	BUTMENT-
17				· ·
18 NOT IN USE  19 12 200 C/C  19a 12 200 C/C  20 300 12 150 C/C  21 150 12 150 C/C  22 — 10 6 NOS.  23 10 2 LEGGED 3 NOS.(HORI.)  24 600 12 150 C/C  25 10 10 150 C/C	16	004	16	150 C/C
19	17	400	16	150 C/C
19a 12 200 C/C  20 300 12 150 C/C  21 150 12 150 C/C  22 — 10 6 NOS.  23 10 400 C/C 2 LEGGED 3 NOS.(HORI.)  24 600 12 150 C/C  25 9 10 150 C/C	18	NO	OT IN US	SE .
20 300 12 150 C/C  21 150 12 150 C/C  22 — 10 6 NOS.  23 10 2 LEGGED 3 NOS.(HORI.)  24 600 12 150 C/C  25 10 10 150 C/C	19		12	200 C/C
20 300 12 150 C/C  21 150 500 12 150 C/C  22	19a		12	200 C/C
21	20		12	150 C/C
23 10 400 C/C 2 LEGGED 3 NOS.(HORL.)  24 600 12 150 C/C  25 9 10 150 C/C	21		12	150 C/C
23 10 2 LEGGED 3 NOS.(HORI.)  24 600 12 150 C/C  25 9 10 150 C/C	22		10	6 NOS.
25 <u>[x]</u> 10 150 C/C	23		10	
	24	<u></u>	12	150 C/C
28 0 0 16 3 NOS.	25	150	10	150 C/C
	28	300	16	3 NOS.

- 1. ALL DIMENSIONS ARE IN MILLIMETERS, LEVELS ARE IN METERS AND CHAINAGES ARE IN KILOMETERS UNLESS OTHERWISE MENTIONED.
- 2. DIMENSIONS ARE NOT TO BE SCALED, ONLY WRITTEN DIMENSIONS SHALL BE FOLLOWED.
- 3. THE CARRIAGEWAY OF PROPOSED BRIDGE IS DESIGNED AS PER IRC : 6-2017.
- 4. ADEQUATE LINKS SPACER BARS ETC SHALL BE PROVIDED FOR PROPER POSITIONING OF REINFORCEMENT.
- 5. LAP JOINT SHALL BE PROVIDED IN STAGGERED MANNER &NOT MORE THAN 50% BAR SHALL BE LAPPED AT ANY SECTION.
- 6. BOND LENGTH SHALL BE 50 TIMES DIA OF BAR & LAP LENGTH SHALL
- 7. ABUT. CAP TOP LEVEL AND PEDESTAL HEIGHT MAY BE VARIES AFTER DESIGN OF

### GRADES, MATERIAL TYPES & ETC.:-

a)	RUU URASH BARRIER	M4U
b)	SUBSTRUCTURE / FOUNDATION	M35
	APPROACH SLAB	
	ABUTMENT CAP	
	PEDESTAL	
	PCC	
	SEISIMIC ZONE	

### .50MM THK.

i) STEEL/HYSD BARS (CONFIRM TO IS:1786).....Fe500D.

#### CLEAR COVER:-

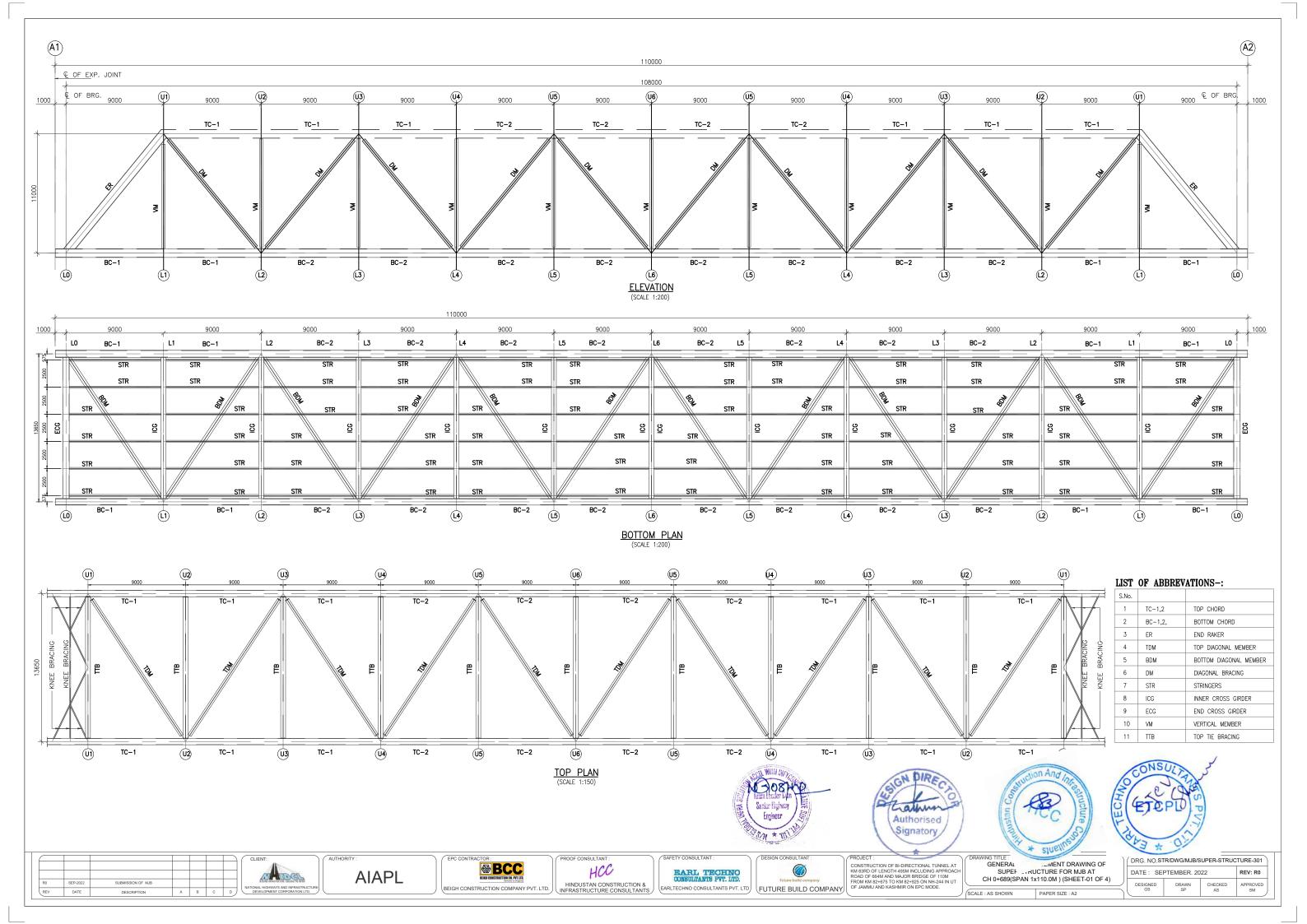
u)	NCC CNASH BARNER	
b)	FOUNDATION	75mm
c)	RCC ABUTMENT SHAFT (EARTH FACE)	.75mm
d)	RCC ABUTMENT SHAFT (NON-EARTH FACE)	40mm
e)	ABUTMENT CAP	50mm
f)	DIRT WALL	.50mm
a)	APPROACH SLAB	50mm

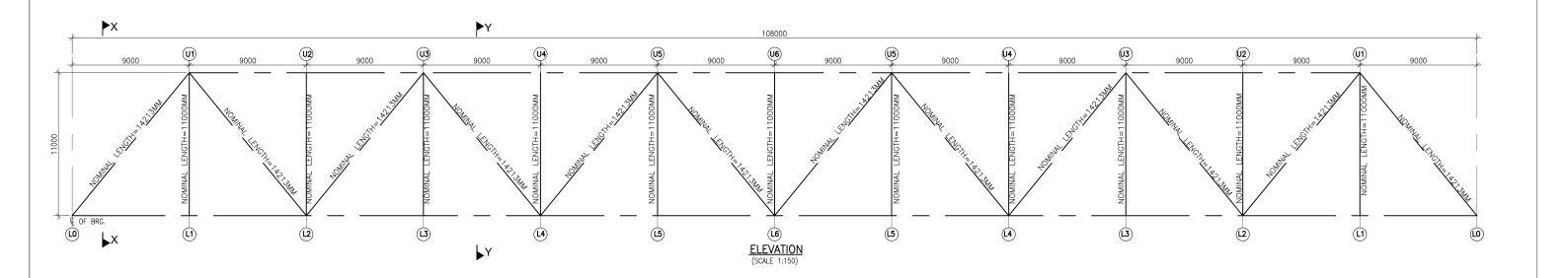
### SPECIAL NOTES:

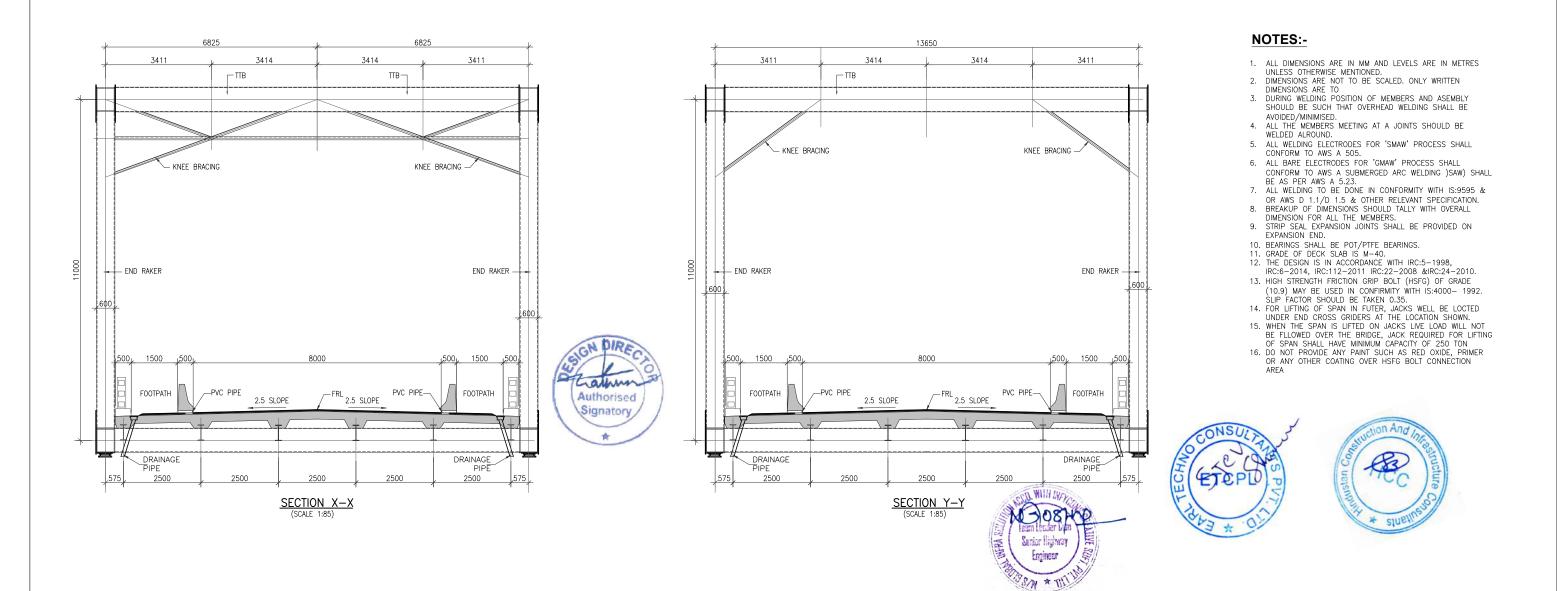
- 01 "SAFE BEARING PRESSURE CONSIDERED IN DESIGN IS 70 T/m2 AND THE SAME SHALL BE VERIFIED AT SITE BEFORE EXECUTION OF WORK."
- 02 "PLATE LOAD TEST SHALL BE DONE AT SITE."

REINFORCEMENT DETAILS OF ABUTMENT A2

DRG. NO.STR/DWG/MJB/REINF./ABUT.-A2/204 DATE: SEPTEMBER. 2022 APPROVED CHECKED SM







SAFETY CONSULTANT

PROOF CONSULTANT

HCC

BCC

BEIGH CONSTRUCTION COMPANY PVT. LTD.

AUTHORITY

ADOUNAUS.

**AIAPL** 

DESIGN CONSULTAN

EARLTECHNO CONSULTANTS PVT. LTD

CONSTRUCTION OF BI-DIRECTIONAL TUNNEL AT KM 83RD OF LENGTH 495M INCLUDING APPROACH ROAD OF 664M AND MAJOR BRIDGE OF 110M FROM KM 82-675 TO KM 82-925 ON NH-244 IN UT OF JAMMU AND KASHMIR ON EPC MODE.

GENERAL ARRANGEMENT DRAWING OF

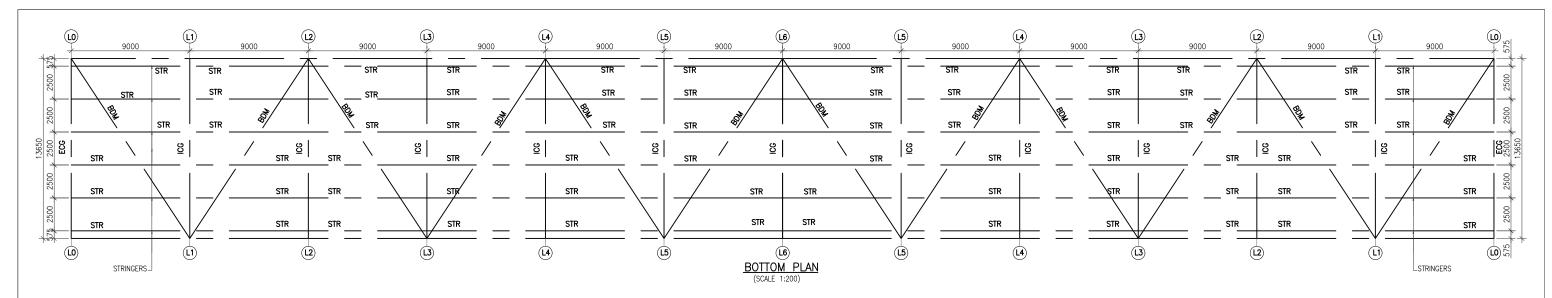
SUPER STRUCTURE FOR MJB AT CH -0+689

(SPAN 1x110.0M) (SHEET-02 OF 04)

DRG. NO.STR/DWG/MJB/SUPER-STRUCTURE-301

REV: R0

DATE: SEPTEMBER. 2022



S.NO.	01.	02.	03.	04.	05.	06.	07.	08.
MEMBER MRK.	BOTTOM CHORD (BC-1)	BOTTOM CHORD (BC-2) L2-L3,L3-L4,L4-L5,L5-L6	TOP CHORD (TC-1)	TOP CHORD (TC-2)	VERTICAL MEMBER (VM)	TOP DIAGONAL MEMBER (TDM)	STRINGERS (STR)	INNER CROSS GIRDER (ICG)
SHAPE	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	600 	600 7 000 150 BATTEN 12MM THK.	600 10 00 150 BATTEN 12MM THK.	13 08	600 17 16 18 BATTEN 12MM THK.	550	700
WEB	① 20	4 22	⑦ 20	① 20	① 20	16 18	19 28	22 28
TOP FLANGE	② 18	⑤ 20	8 18	18	12	17 12	20 20	23 28
BOTTOM FLANGE	③ 12	6 12	9 12	12	15 12	18 12	20 20	24 28



S.NO.		09.		10.		11.		12.		13.	14.
MEMBER MRK.	END C	CROSS GIRDER (ECG)	E	END RAKER (ER)	TOP	TIE BRACING (TTB)		OTTOM DIAGONAL MEMBER (BDM)	DIAG	GONAL MEMBER (DM)	KNEE BRACING
SHAPE		25 00 00 00 00 00 00 00 00 00 00 00 00 00	+	600 28 150 BATTEN 12MM THK.		275 - 32 9	-         	600 35 36 BATTEN 12MM THK.	l <del>-</del>	600 57 BATTEN 12MM THK.	10
WEB	25	32	28	20	31)	18	34)	16	37)	22	Carlotte Control
TOP FLANGE	26	32	29	22	32	12	35)	12	38	22	ISA = AVX150KQ &
BOTTOM FLANGE	27	32	30	22	33	12	36	12	39	22	Senior Highway

#### LIST OF ABBREVATIONS-:

шот	OI ADDIVE	ATIOND .
S.No.		
1	TC-1,2	TOP CHORD
2	BC-1,2,	BOTTOM CHORD
3	ER	END RAKER
4	TDM	TOP DIAGONAL MEMBER
5	BDM	BOTTOM DIAGONAL MEMBER
6	DM	DIAGONAL BRACING
7	STR	STRINGERS
8	ICG	INNER CROSS GIRDER
9	ECG	END CROSS GIRDER
10	VM	VERTICAL MEMBER
11	TTB	TOP TIE BRACING



#### **NOTES:-**

- 1. ALL DIMENSIONS ARE IN MM AND LEVELS ARE IN METRES
- UNLESS OTHERWISE MENTIONED.

  2. DIMENSIONS ARE NOT TO BE SCALED. ONLY WRITTEN DIMENSIONS ARE TO BE FOLLOW.
- 3. FOR ERECTION / LAUNCHING SCHEME SEE SEPARATE
- DRAWING.

  4. ALL BUTT WELDED ARE TO BE EXAMINED RADIOGRAPHICALLY OR ANY EQUALLY EFFECTIVE NON DESTRUCTIVE TEST METHOD.

- METHOD.

  5. ALL WELDS TO BE MADE BY APPROVED WELDING PROCEDURES.

  6. FABRICATION SHALL BE DONE AS PER IRC: 24–2010.

  7. FILLET WELDS ARE OF LEG SIZE 6MM MINIMUM AND AS PER IS:CODE 9595–1996.

  8. ALL OBTUSE ANGLE CUTTING SHOULD BE DONE IN PROPER
- SHAPE & WITHOUT DAMAGE.

  9. OVERHANGING MEMBER TO BE SUITABLY SUPPORTED TO AVOID DISTORTION DURING TRANSPORTATION.
- ALL WELDS SHALL BE IN ONE GO (CONTINUOUS) UNLESS SPECIFIED OTHERWISE.

- SPECIFIED OTHERWISE.

  11. FOR DESIGN OF BRIDGE SEISMIC ZONE—IV IS CONSIDERED.

  12. ALL STRUCTURAL STEEL PLT SHALL BE E350 CONFORMING
  TO IS 2062—2006.

  13. FOR FABRICATION, WORKMANSHIP, INSPECTION & TESTING
  PROTECTION AGAINST CORROSION ETC, RELEVANT PROVISION
  OF IRC 24—2010 SHALL BE FOLLOWED.

  14. CONSTRUCTION STAGE SCHEME SHALL BE PROVIDED BY
  CONTRACTOR AND CONSTRUCTION SHALL BE VERIFIED BY
  DDC REFORE FABRICATION.
- DDC BEFORE FABRICATION 15. CONGESTION FACTOR IS NOT CONSIDERED.

#### **WELDING NOTES:-**

- 1. WELDING ELECTRODES SHALL CONFIRM IS 814 OR IS 1395
- ALL WELDING ELECTRODES OR 'SMAW' PROCESS SHALL CONFORM A 5.5 FOR HT & AWS A 5.1 FOR MS.
- 3. METAL ARC WELDING SHALL CONFORM TO IS:9595 & 816/
- 4. FOR SCHEME & SYMBOLS OF WELDING REFER IS:813-1986.
  5. ALL WELDING TO BE DONE IN CONFIRMITY WITH IS:9595 & OR AWS D 1.1/D1.5& OTHER RELEVANT SPECIFICATION.















Engineer

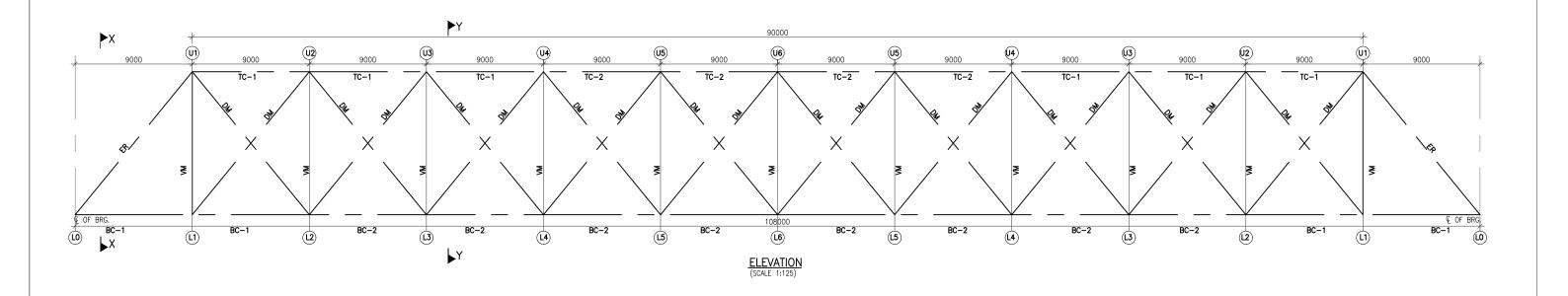
PROJECT PROJECT :

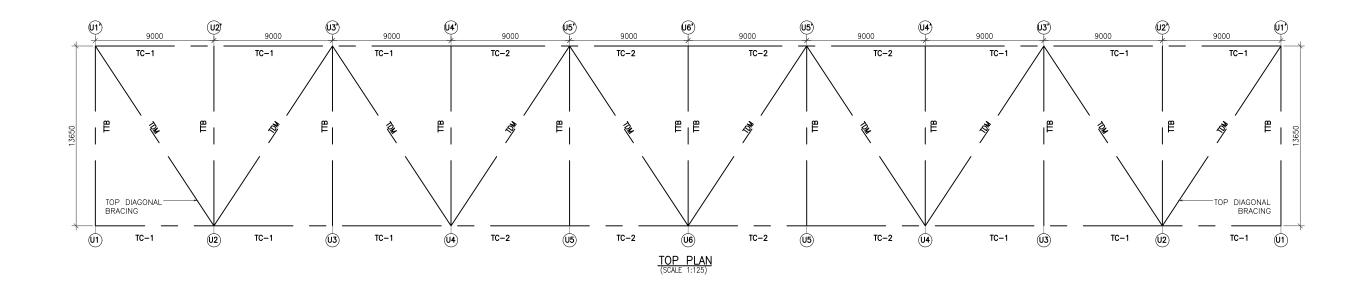
CONSTRUCTION OF BI-DIRECTIONAL TUNNEL AT KM 83RD OF LENGTH 495M INCLUDING APPROACH ROAD OF 664M AND MAJOR BRIDGE OF 110M FROM KM 82-675 TO KM 82-925 ON NH-244 IN UT OF JAMMU AND KASHMIR ON EPC MODE.

GENERAL ARRANGEMENT DRAWING OF SUPER STRUCTURE FOR MJB AT CH -0+689

DRG. NO.STR/DWG/MJB/SUPER-STRUCTURE-301

	DATE: SE	REV: R0						
$\preceq$	DESIGNED GS	DRAWN SP	CHECKED AS	APPROVED SM				













R0	SEP-2022	SUBMISSION OF MJB				
REV	DATE	DESCRIPTION	А	В	С	D)









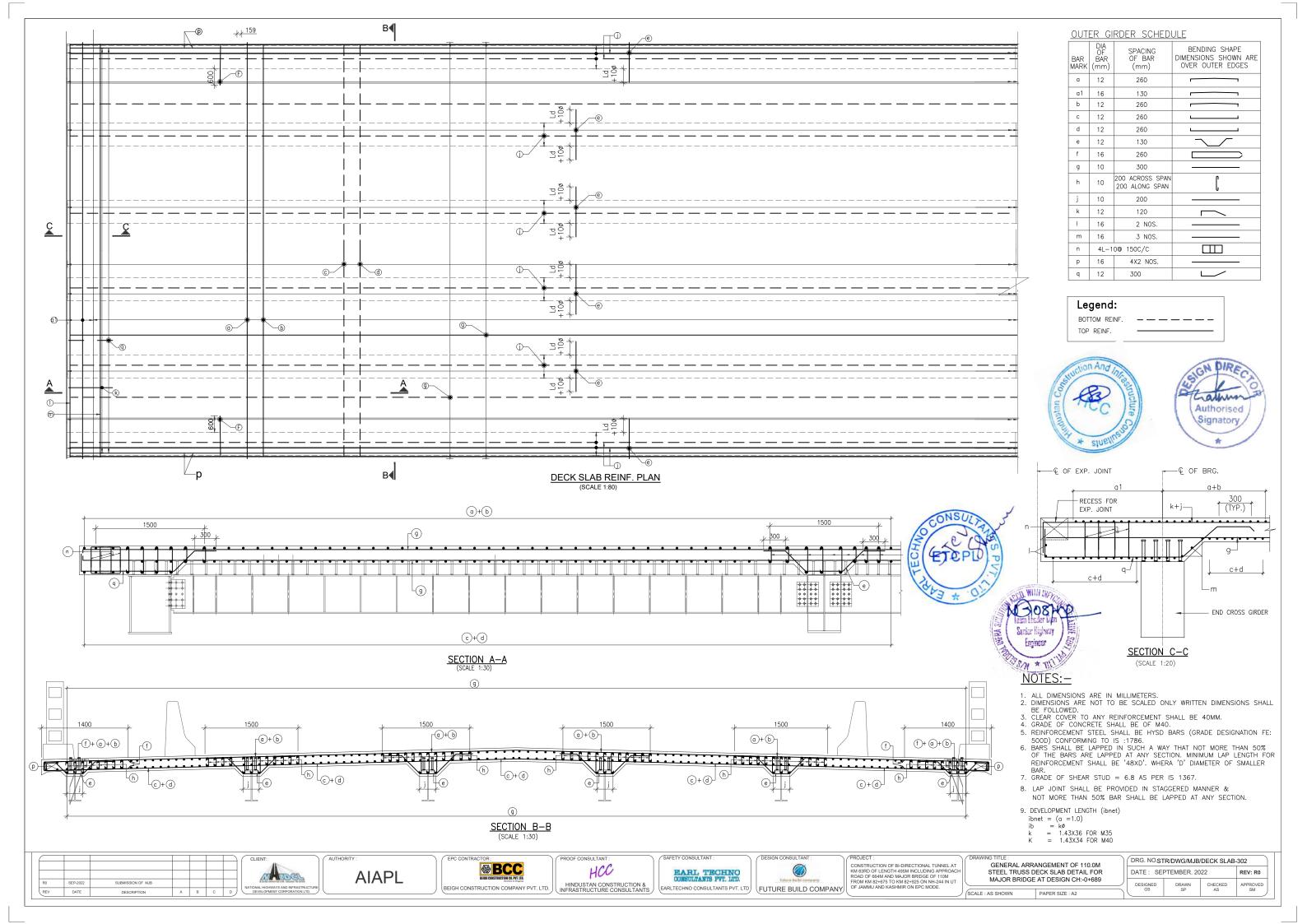




1	PROJECT:	١.
	CONSTRUCTION OF BI-DIRECTIONAL TUNNEL AT KM 83RD OF LENGTH 495M INCLUDING APPROACH	
	ROAD OF 664M AND MAJOR BRIDGE OF 110M	I
	FROM KM 82+675 TO KM 82+925 ON NH-244 IN UT	ľ

DRAWING TITLE :					
SUPER STRUCTUR	NGEMENT DRAWING OF RE FOR MJB AT CH -0+689 DM ) (SHEET-04 OF 04)				
SCALE : AS SHOWN	PAPER SIZE : A2				

	DRG. NO.ST	R/DWG/MJB/S	SUPER-STRU	CTURE-301	
	DATE: SE	DATE: SEPTEMBER. 2022			
$\preceq$	DESIGNED GS	DRAWN SP	CHECKED AS	APPROVED SM	





EPC Contracto

Beigh Construction Company Pvt. Ltd Plot No : 4, Wave Mall, Bypass Road, Narwal Jammu

# Construction of Bi Directional Tunnel at " KM 83" of length 495m including Approach Roads of 664 m and a Major Bridge of 110m from Km 82 + 675 to Km 82 + 925 on NH-244 in Jammu & Kashmir on EPC Mode

#### **PAVEMENT DESIGN**

21-12-2020





Central, oficinas y laboratorio: Pasaje Bisbal, 6 - 3°. 28028 - MADRID. Ver Mapa.. T: (+34) 917131390 www.seclindia.com



1<sup>st</sup> Floor, Al-Farooq Building, Jawahar Nagar, Srinagar-08 (J&K) ⊘(+91)194-2310344,⊠space@seclindia.com







IRC:58-2015 Guidlines of						
Plain jointed Rigid Pave	Plain jointed Rigid Pavements for Highways					
Design of Slab thicn	Design of Slab thicness for pavement					
Criteria : Concrete pavement bounded with Dry lean concrete						
Specification: Two Lane Two Way(2L2W)-Lane width: 3.5 r	n : Spacing of Contraction Joint : 4	l.5m				
Design Parameters	Value adopted with units	Refrence				
A. Modulus subgrade Reaction						
CBR ( Compacted Subgrade)	15%	Site Data				
Modulus of subgrade-( strength of subgrade)	62MPa/m	Table-2(IRC:58-2015)				
Thicknness of granular base (I&II)	200mm	Contract Document				
DLC sub base thickness (adopted) (M-6.5 to M7.5) min strength 7N/mm after 7						
days	150mm	Contract Document				
Effective Modulus of subgrade (subgrade+GSB+DLC) -Interploation	293MPa/m	Table-4(IRC:58-2015)				
B. Selection of Flexural Strength						
28 days compressive strength of Cement concrete for PQC	> 40 Mpa ( Target strength after 90days 48MPa) Ft= Fck+1.65*5	IS:10262 (2009) &IS :456200				
28 days flexural strength of Cement concrete for PQC	4.4 to 4.5 Mpa (4.84 Mpa after 90days)	IS:10262 (2009) &IS :456200				
C. Design Trafic criteria:						
Design Period	30 years	IRC:58-2015/ Contract document				
Design Traffic	20msa	Contract Document				
Hence, design number of axle load repetitions for bottom-up cracking analy	rsis = 20000000					
D. Cumulative Fatigue Damage (CFD) analysis for Bottom-Up Cracking (BUC)and Top-Down Cracking (TDC) and Selection of Slab Thickness						
Effective modulus of subgrade reaction of foundation, k	62MPa/m					
Elastic Modulus of concrete, E	28000 Mpa					
Poisson's ratio of concrete, µ	0.15					
Unit weight of concrete, γ	25 kN/m3					
Design flexural strength of concrete	4.8 Mpa					
Max. day-time Temperature Differential in slab (for bottom-up cracking)	15.8 Degree C	Table-1(IRC:58-2015) for thickness range of 300mm-400mm (location : J&K)				
Night-time Temperature Differential in slab (for top-down cracking) =day-time differential	12.9 Degree C					
Lateral placement factor (0.25 for 2 lane 2 way)	0.25					
Factor for selcetion of traffic for BUC analysis (for six hours period during day)	0.25					
Other Details						
Shoulders : Tied concrete shoulders	Yes ( paved shoul	ders)				







Flextural strength of Concrete, Mpa			4.4145	Spacing of Contra	ction Joints, m	4.0
Effective modulus of subgrade reaction of DLC subbase, MN/m3				Width of slab, m		3.5
Elastic Modulus of Concrete, MPa				No of lanes in both directions		2
Poisson's ratio				Type of carriagewa		Divided
Coefficient of thermal expansion of concr	ete, / 0C			Trial Thickness of		290
Tyre pressure, kPa				Radius of relative	stiffness, m	0.676
Growth rate of traffic				Growth Factor		103.40
Design Life, Years			30 Lane Distribution Factor		0.75	
Proportion of trucks plying along edge			0.34 Directional Distribution Factor			0.54
	Inc. of A. L.	l. (	le	lou put	IAU	D
Axle Load, t LF*Axle Load, t	No. of Axles	stress, kg/cm2 Single Axle With S	Expected No.	Stress Ratio	Allowable No.	Damage Ratio
16 1			o O	0.37	Unlimited	0.0
14 1		15.0	42891		Unlimited	0.0
12 1		13.4	111162		Unlimited	0.0
10 1		11.6	370668		Unlimited	0.0
8 1		9.8	2604818		Unlimited	0.0
	7 1536	7.8	7982281		Unlimited	0.0
	5 2093	5.7	10879141		Unlimited	0.0
	2 274	3.3	1426296		Unlimited	0.0
2	214	Single Axle with D		0.07	Onlimited	0.0
24 28.	3 2	24.73	12690	0.55	126167	0.101
22 26.		23.26	12690		367648	0.035
20 2		21.72	819029		2004954	0.409
18 21.		20.17	221403		90733912	0.002
16 19.		18.45	956728		Unlimited	0.002
14 16.		10.10	2869137		Unlimited	0
12 14.			4627569		Unlimited	0
10 1			2273248		Unlimited	0
10		Tandem A		0.00	Oriminicoa	Ů
40 48 8 16.76			42891	0.37	Unlimited	0
36 43.		15.53	446756	0.35	Unlimited	0
32 38.		14.23	458984	0.32	Unlimited	0
28 33.		20	1231501		Unlimited	0
24 28.			3317578		Unlimited	0
20 2			3870601		Unlimited	0
16 19.			1514834		Unlimited	0
		Tridem A				
48 57.	5 15	21.54	78871		2646545	0.030
44 52.	3 207	20.06	1073331	0.45	151766641	0.007
40 4	3 45	18.55	235089	0.41	Unlimited	0.000
						0.58







#### Since summation CFD is less than 1, i.e 0.58, Hence safe n ok

#### I. Thickness Design:

Considering pavement option as Concrete bound pavement bounded to Dry lean concrete layer (DLC), 7days 9-10 MPa strength, DLC is imperative for the said case of Rigid pavement. Cement content in Dry lean concrete must not be less than 170 kg/cum. Separation membrane is recommended to be placed between the base and the concrete slab (PQC) to make the interface condition smooth. A de-bonding interlayer ofpolythene sheet white or transparent or any other colour having a minimum thickness of 125 micron is recommended as per the current practice in India. Granular sub base of 200mm thickness above sub grade is recommended.

Assuming that doweled transverse joints and tied concrete shoulders will be provided, the thickness of slab required for the given traffic conditions and other design data = 0.30m

E(Concrete)=30000MPa E(DLC)= 13600 MPa; Poisson's ratio(con)= 0.15; Poisson's Ration (sub)= 0.20

Provide DLC thickness of 0.15m (DLC of 9-10 MPa strength at 7days is considered)

Depth of neutral axis (computed using equation11 of IRC:58-2015) d= 0.19m

$$d = \frac{0.5(h_1^2) + \left(\frac{E_2}{E_1}\right) h_2(h_1 + 0.5h_2)}{h_1 + \left(\frac{E_2}{E_1}\right) h_2} \qquad \dots 11$$

Flexural Stiffness of slab proposed to be placed over DLC (Equation 12 of IRC:58-2015)= 83.78MN.m

Flexural stiffness (1, PQC) = 
$$\frac{E_1 \left( \left( \frac{h_1^3}{12} \right) + h_1 (d - 0.5h_1)^2 \right)}{1 - \mu_1^2} \dots 12$$

Flexural Stiffness of DLC (Equation 13 of IRC:58-2015) = 34.77 MN.m







Flexural Modulus (2, DLC) = 
$$\frac{E_2\left[\frac{\left(\frac{E_2}{E_1}\right)h_2^3}{12} + \left(\frac{E_2}{E_1}\right)h_2\left(h_1 + \frac{h_2}{2} - d\right)^2\right]}{(1 - \mu_2^2)} \qquad \dots (13)$$

Combined stiffness of Slab and DLC = 118.55 MN.m Stiffness of design slab of 0.3m thickness (Equation 10 of IRC:58-2015) =69.05MN.m

$$\frac{EI}{1-\mu^2} = \frac{Eh^3}{12(1-\mu^2)} \qquad ... (10)$$

**Combined stiffness is more than Design Stiffness requirement. Hence Ok: Conclusion:** Adopt 300mm thickness of PQC with 150 mm DLC and 200mm GSB

#### II. Design of Dowel bars:

Slab thickness: 300mm Joint width = 20mm

Radius of Relative stiffness = 1035.3 mm

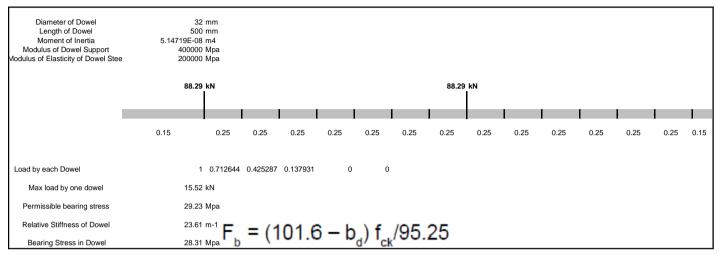
E for dowel bar =  $2 \times 10^5 MPa$ 

Modulus of dowel support, k<sub>mds</sub>= 415000 MPa/m









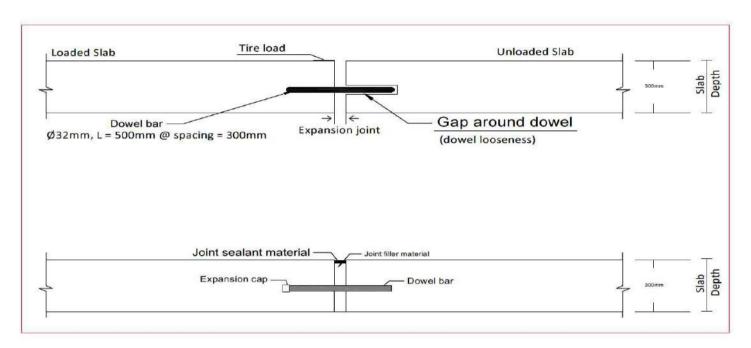
Since Bearing stress in dowel bar is less than permissible bearing stress in concrete computed using e.15 IRC:58-2015.

Dowel bars of dia 32 mm, with length 500 mm and spacing 300mm is recommended for the current rigid pavement.









#### **III.** Check for Corner stresses:

Corner stresses have been computed The maximum stress (bending tension)  $\sigma$ c and deflection  $\delta$  c due to the load at corner of a rigid slab is given by Westergaard as:

$$\sigma_c = \frac{3P}{h^2} \Bigg[ 1 - \bigg( \frac{a\sqrt{2}}{\ell} \bigg)^{0.6} \Bigg] \qquad \qquad \text{Where:} \\ k = \text{modulus of subgrade reaction} \\ \ell = \text{radius of relative stiffness} \\ \delta_c = \frac{P}{k\ell^2} \Bigg[ 1.1 - 0.88 \bigg( \frac{a\sqrt{2}}{\ell} \bigg) \Bigg] \qquad \qquad a = \text{load contact radius} \\ P = \text{load}$$

The above equation for sc as modified by Kelly is being used by IRC for computing the wheel load stress at corner







$$\sigma_c = \frac{3P}{h^2} \left[ 1 - \left( \frac{a\sqrt{2}}{l} \right)^{1.2} \right]$$

And is worked out as: Computed using Excel program

Check for Corner Stress		
Axle Load, t	24	
Wheel Load, t	12	
Radius of contact, cm	30.59	
Corner Stress, kg/cm2	17.30	

:

Since , Corner stress is less than Flexural strength of concrete and the pavement thickness of 300mm assumed is **Safe** 

#### IV. Design of Tie Bars

Area of steel required per metre length of joint has been computed using the following equation:

$$A_s = \frac{bfw}{s_{st}} \qquad \dots (16)$$

In which,

A<sub>s</sub> = area of steel in mm<sup>2</sup>, required per m length of joint

b = lane width in metres

f = coefficient of friction between pavement and the subbase/base (usually taken as 1.5)

W = weight of slab in kN/m² and

S<sub>st</sub> = allowable working stress of steel in MPa

As per the provisions of IRC:58-2015, The length of any tie bar should be at least twice that required to develop a bondstrength equal to the working stress of the steel. The formula for estimating the length of tiebar is given as equation 17.







$$L = \frac{2 S_{st} A_{cs}}{B^* P_{pib}}$$
 ... (17)

In which:

L = length of tie bar (mm)

S<sub>st</sub> = allowable working stress in steel (MPa)

 $A_{cs}$  = cross-sectional area of one tie bar (mm<sup>2</sup>)

P<sub>pth</sub> = perimeter of tie bar (mm), and

B\* = permissible bond stress of concrete (i) for deformed tie bars = 2.46 MPa,

(ii) for plain tie bars - 1.75 MPa.

(i). Slab thickness = 0.30 m

(v). Allowable Tensile stress in deformed bar, Sst (MPa)= 200 (IRC:15-2011)

(ii).Lane width (b) = 3.5 m

(vi). Allowable bond stress in deformed  $bar(B^*) = 2.46$ 

(iiii).Coefficient of Friction (f) =1.5

(vii).Dia of tie bar = 12 mm

(iv). Density of concrete( $KN/m^3$ )= 24

(viii). Area of Tie bar= 113.1 mm<sup>2</sup>

### Spacing and Length of Deformed bars: Using Excel developed programme using above equations and parameters

Tie bar design		Deformed bars
Area of tie bar steel, cm2	3.024	1.89
Area of 12 mm tie bar	1.131	1.131
Perimeter of tie bar	3.770	3.770
Spacing, cm	37.400	59.840
Length of tie bar, cm	57.857	63.780







#### **Design Conclusion:**

- I. Provide pavement thickness of 300mm Pavement Quality Concrete ( PQC ) having 28-days Flexural and Compressive Strengths 4.5 MPa and 40 MPa respectively over 150 mm Dry Lean Concrete Subbase with a minimum 7-Day Compressive Strength of 7 MPa with 32 mm diameter Dowel bars of length 500 mm at a spacing of 300mm and deformed Tiebars of 12 mm diameter, 640 mm length at a spacing of 600 mm (c/c).
- II. Provide a drainage layer (GSB) of 200 mm thickness with a drainage coefficient of min. 350 m per day.









### Roadside Drainage

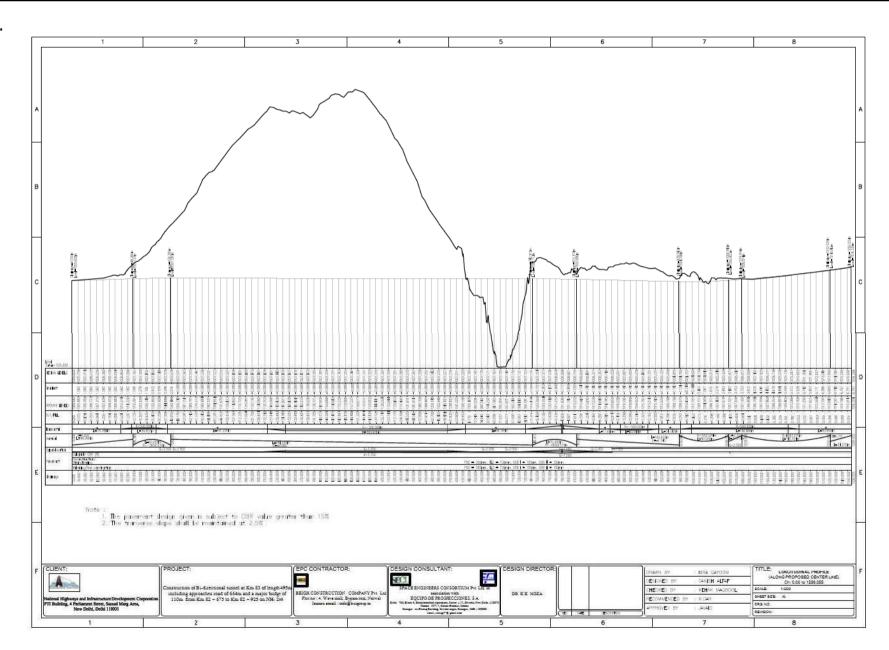
S. No	DESIGN CHAIN	NAGE	LENGTH	DRAIN	TCS TYPE	
3. NO	From	То	LLINGTH	DRAIN	ICS TIPE	
01	0+000	0+065	65	Both Sides	TCS-1	
02	0+065	0+128	63	Both Sides	TCS-1	
03	0+733	0+745	12	One Side	TCS-3	
04	0+745	0+780	35	Both Sides	TCS-1	
05	0+780	0+845	65	One Side	TCS-2	
06	0+845	0+880	35	One Side	TCS-3	
07	0+880	0+935	55	One Side	TCS-3	
08	0+935	0+975	40	One Side	TCS-3	
<u>09</u>	0+975	1+015	40	One Side	TCS-2	
10	1+015	1+080	65	One Side	TCS-3	
11	1+080	1+155	75	One Side	TCS-2	
12	1+155	1+215	60	One Side	TCS-1	
13	1+215	1+240	25	Both Sides	TCS-2	
14	1+240	1+269	29	One Side	TCS-3	







III.







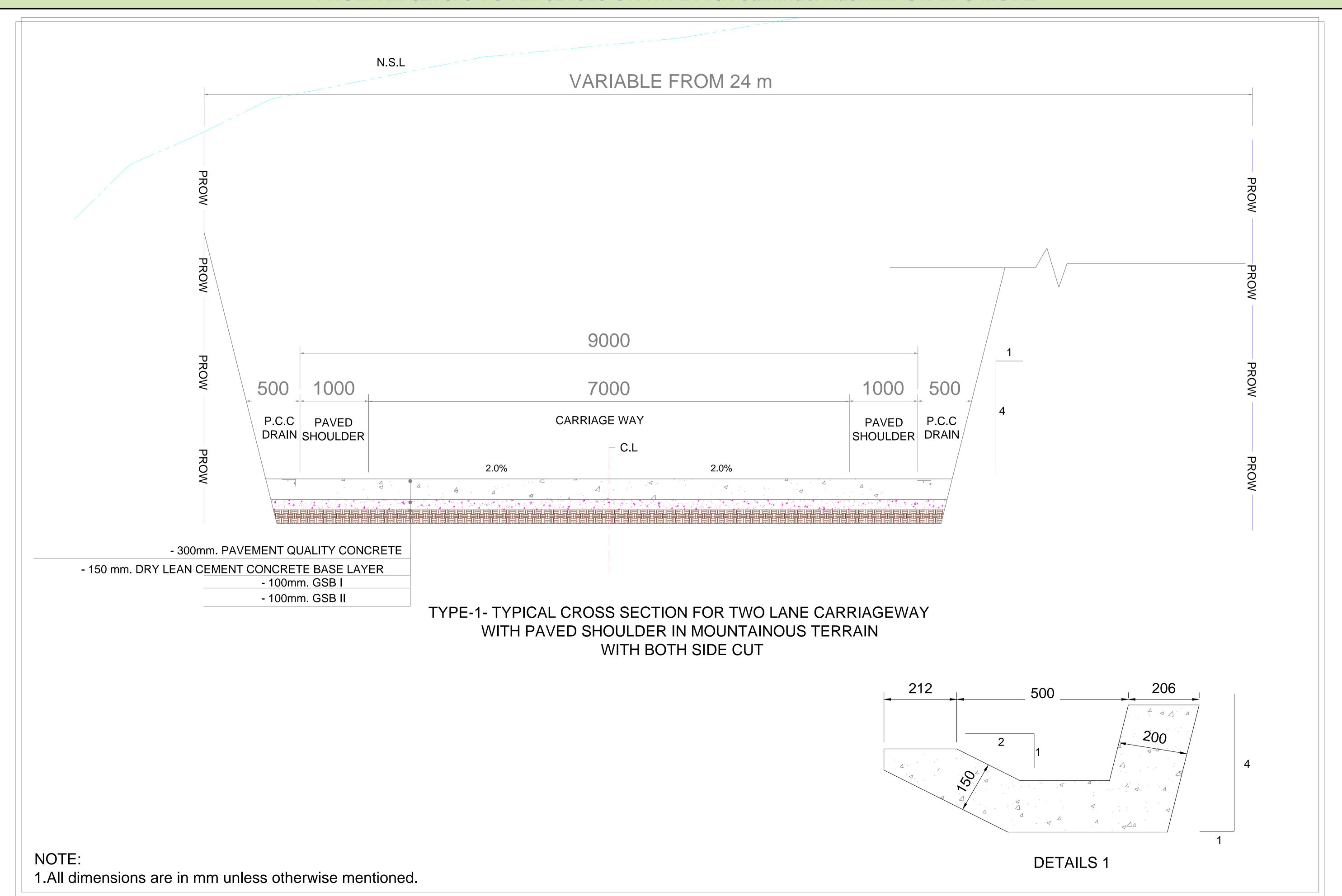


Pavement Quality Concrete (PQC)300 mm
Dry lean concrete (DLC)150mm
GSB -I - 100 mm
GSB -II - 100 mm
Sub grade





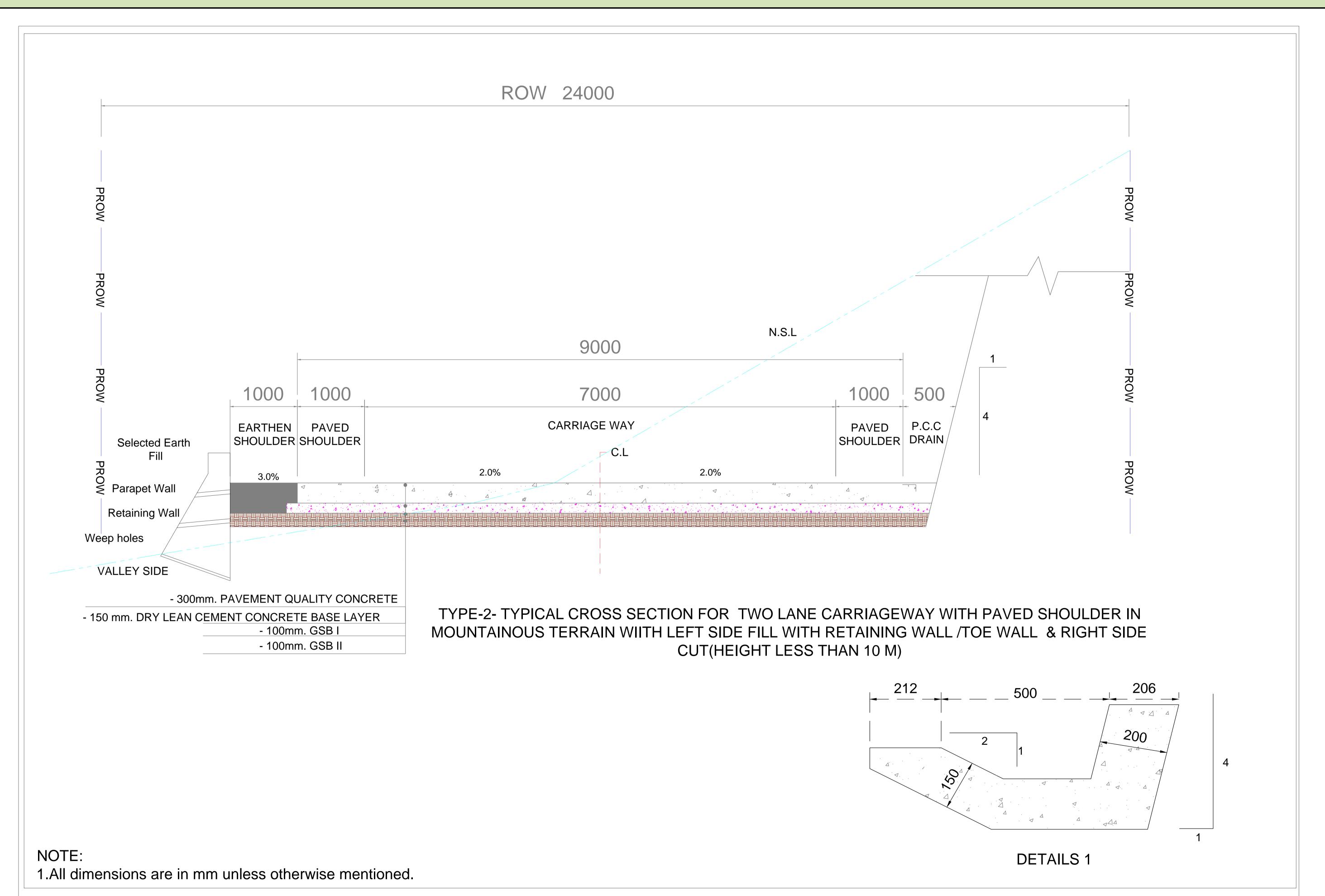








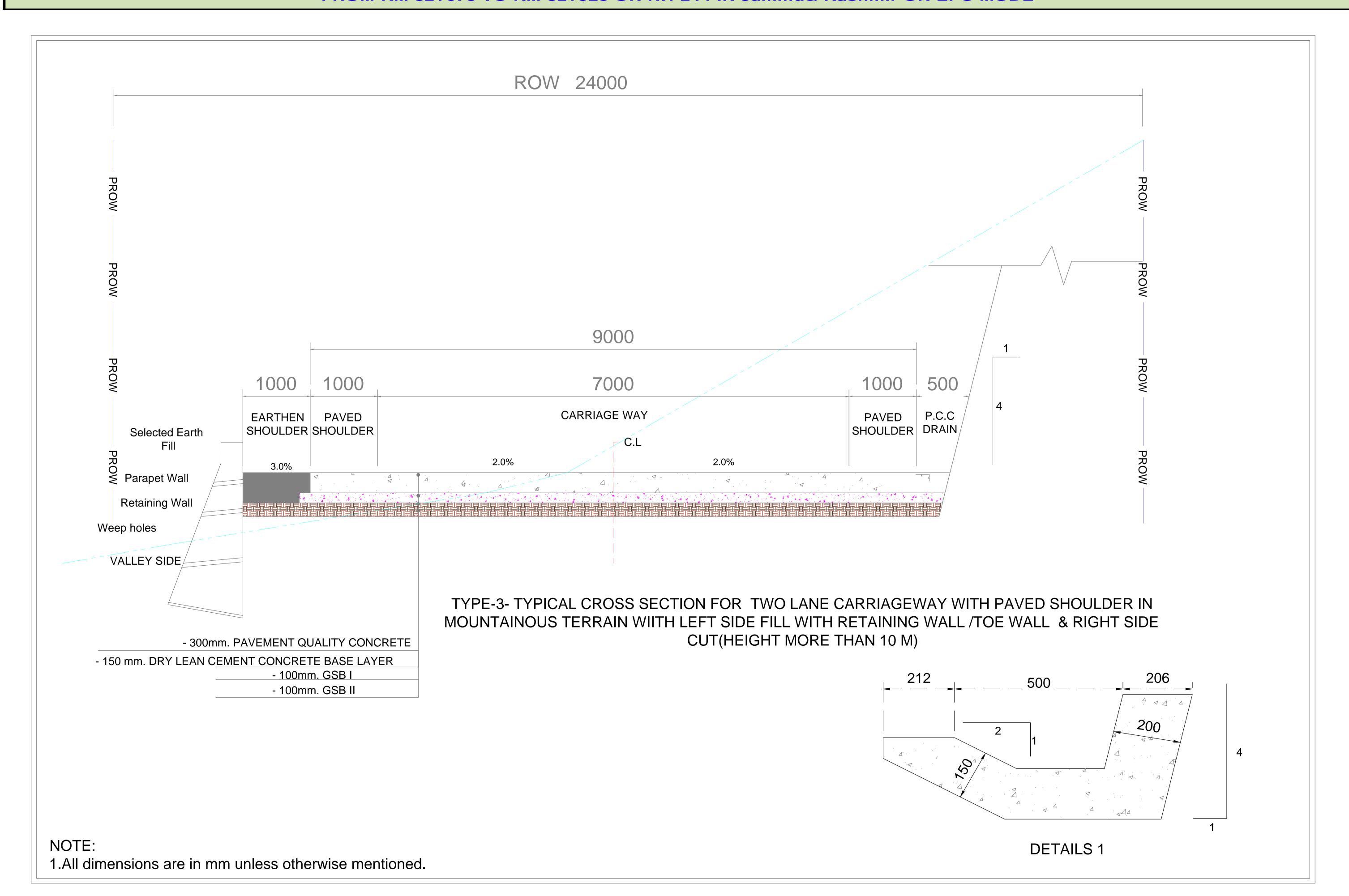


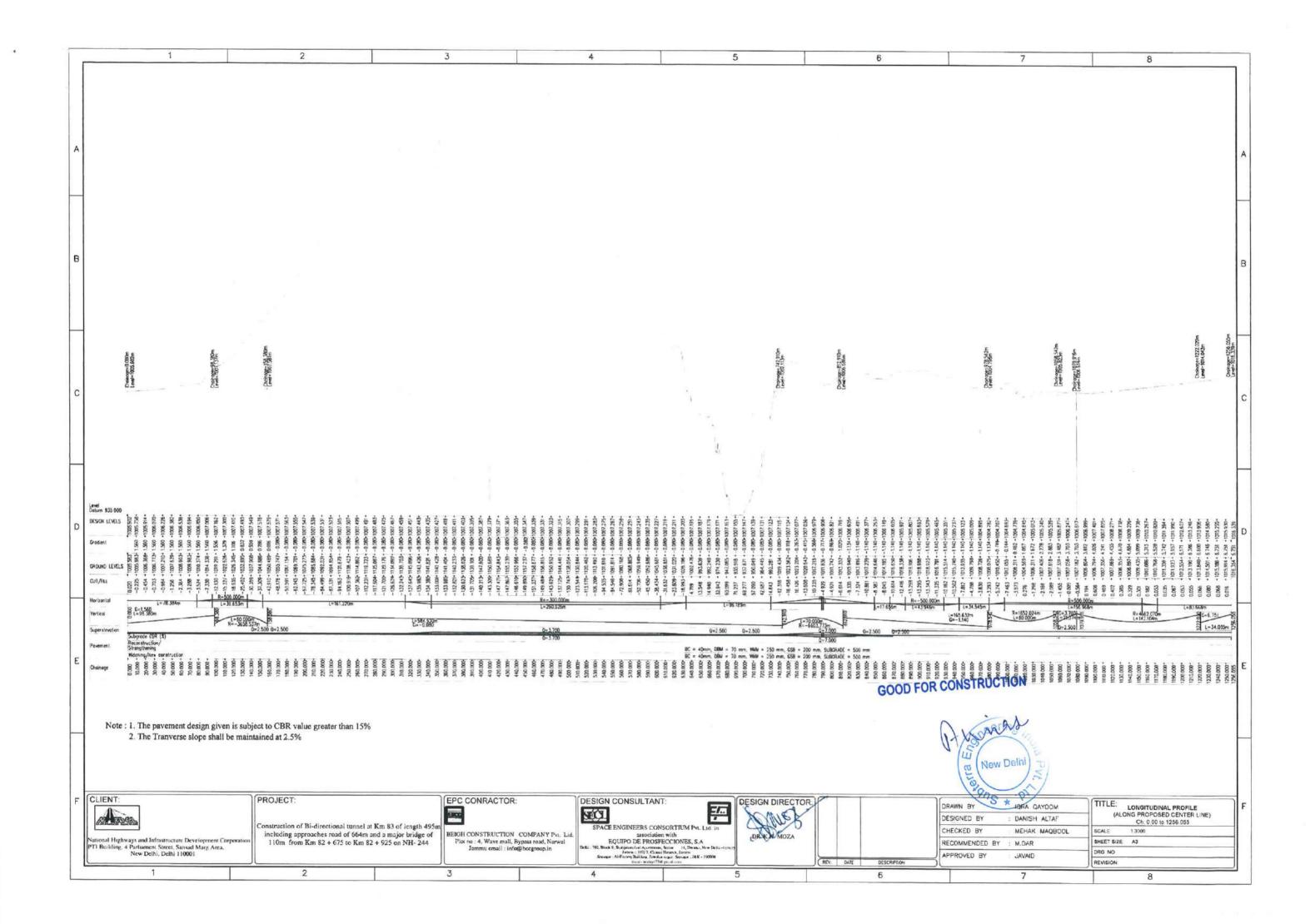


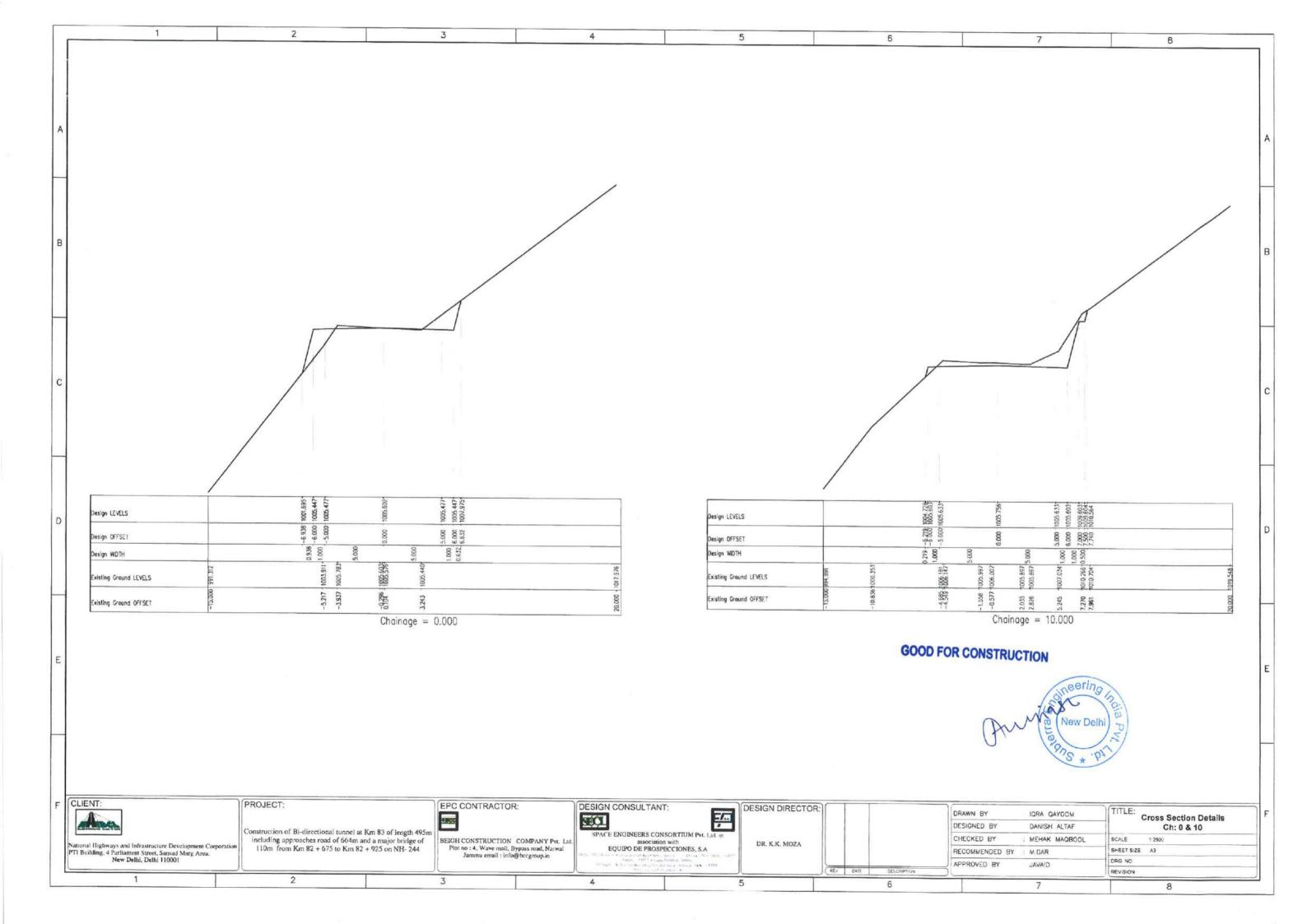


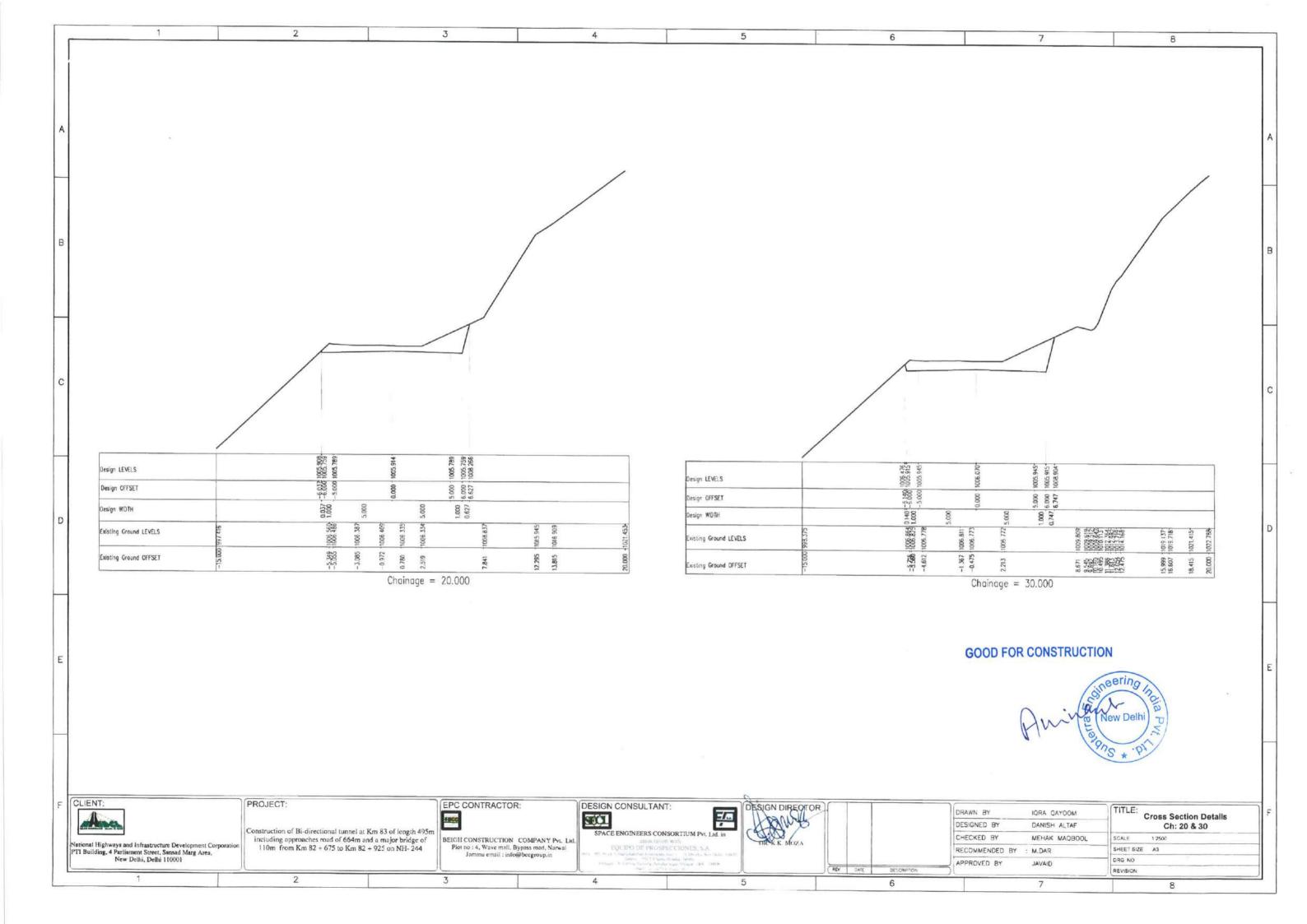


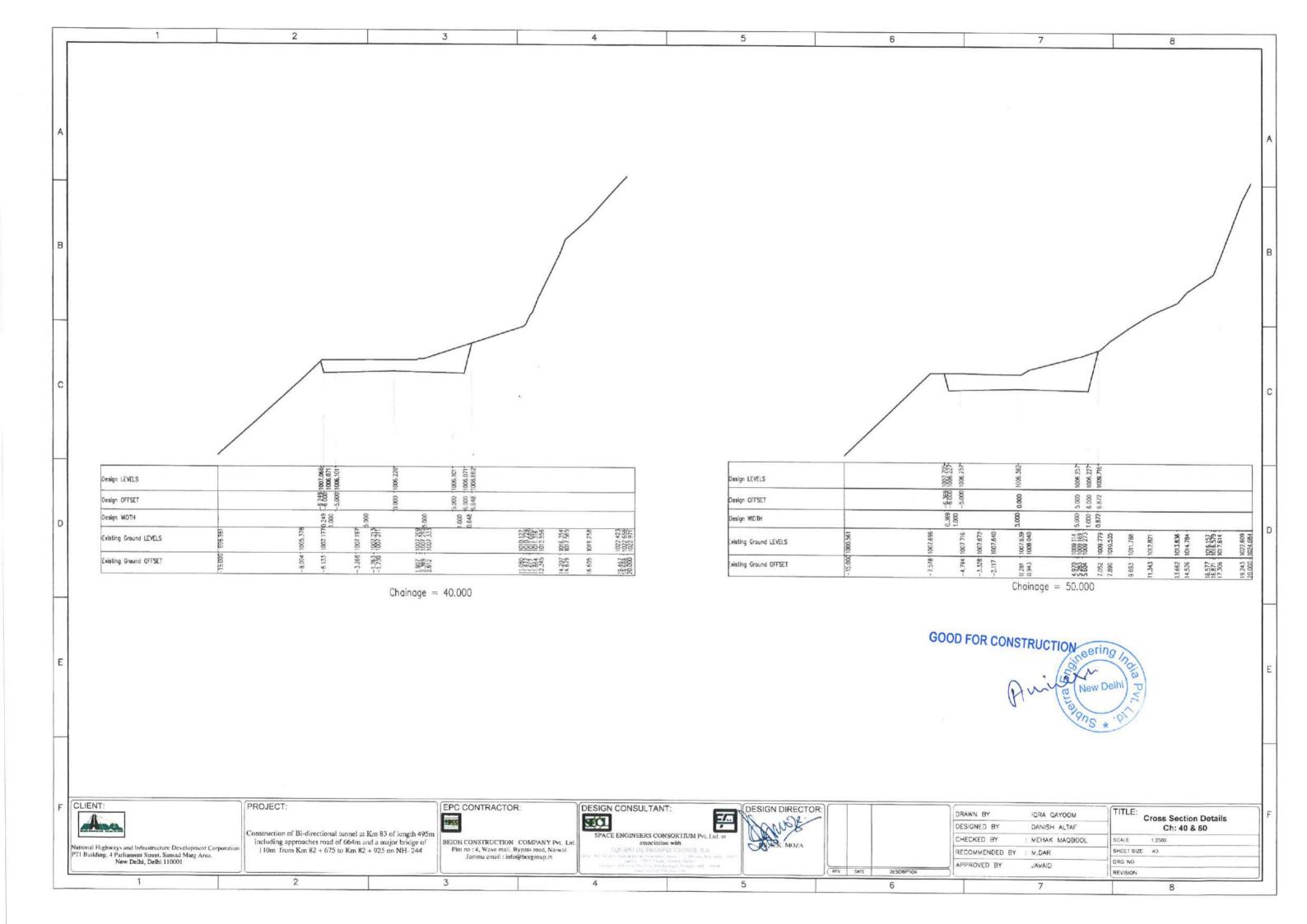


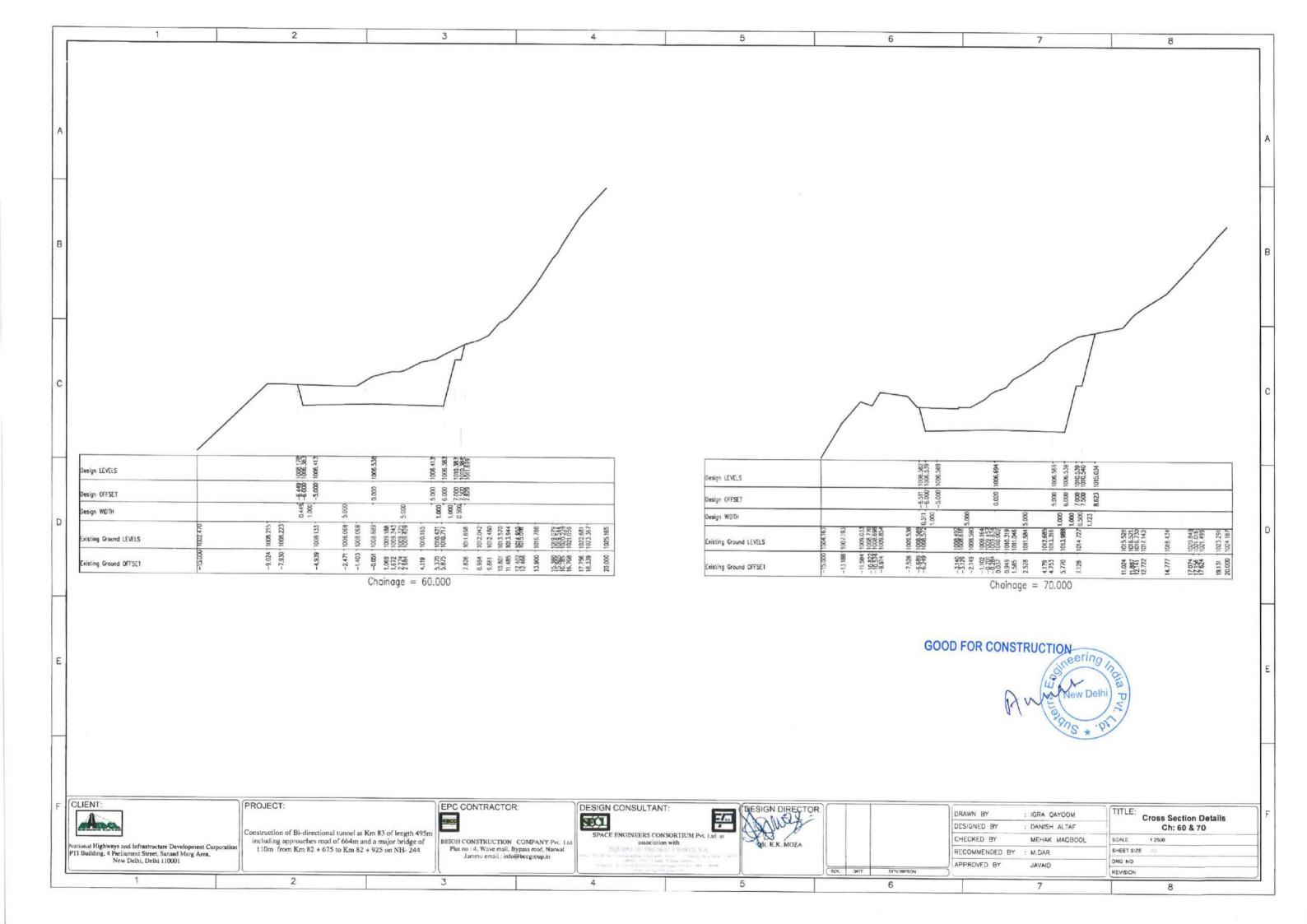


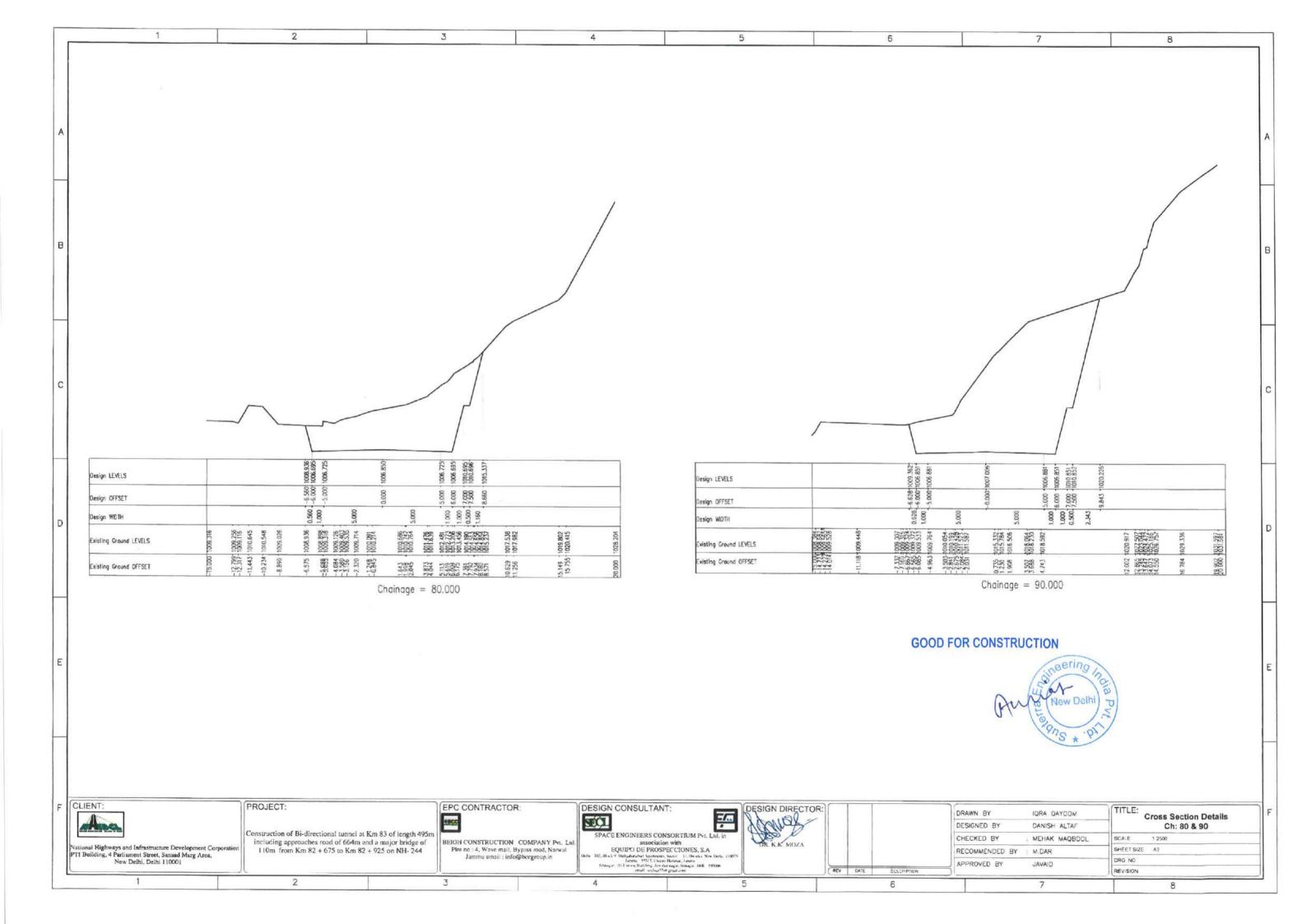


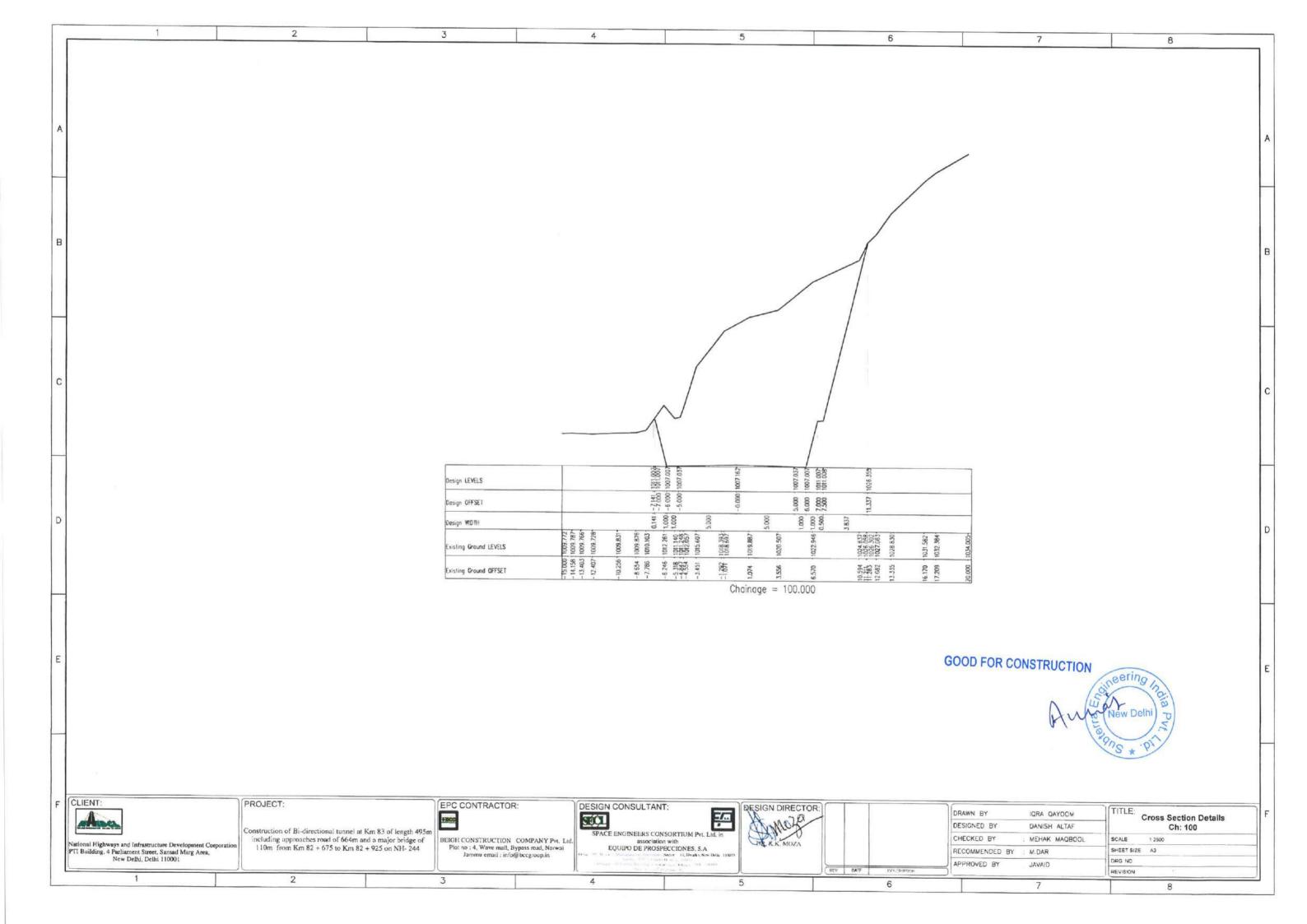


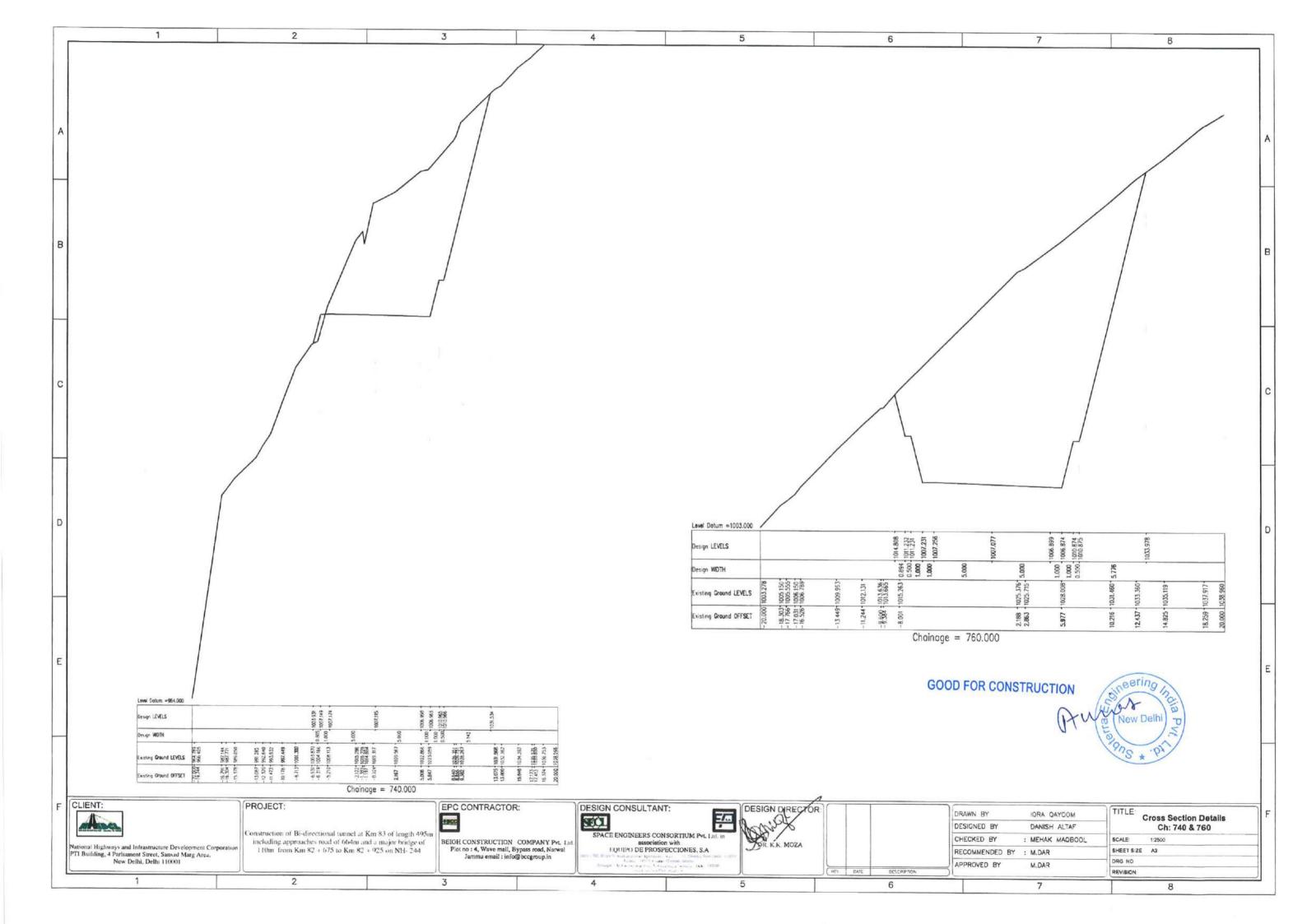


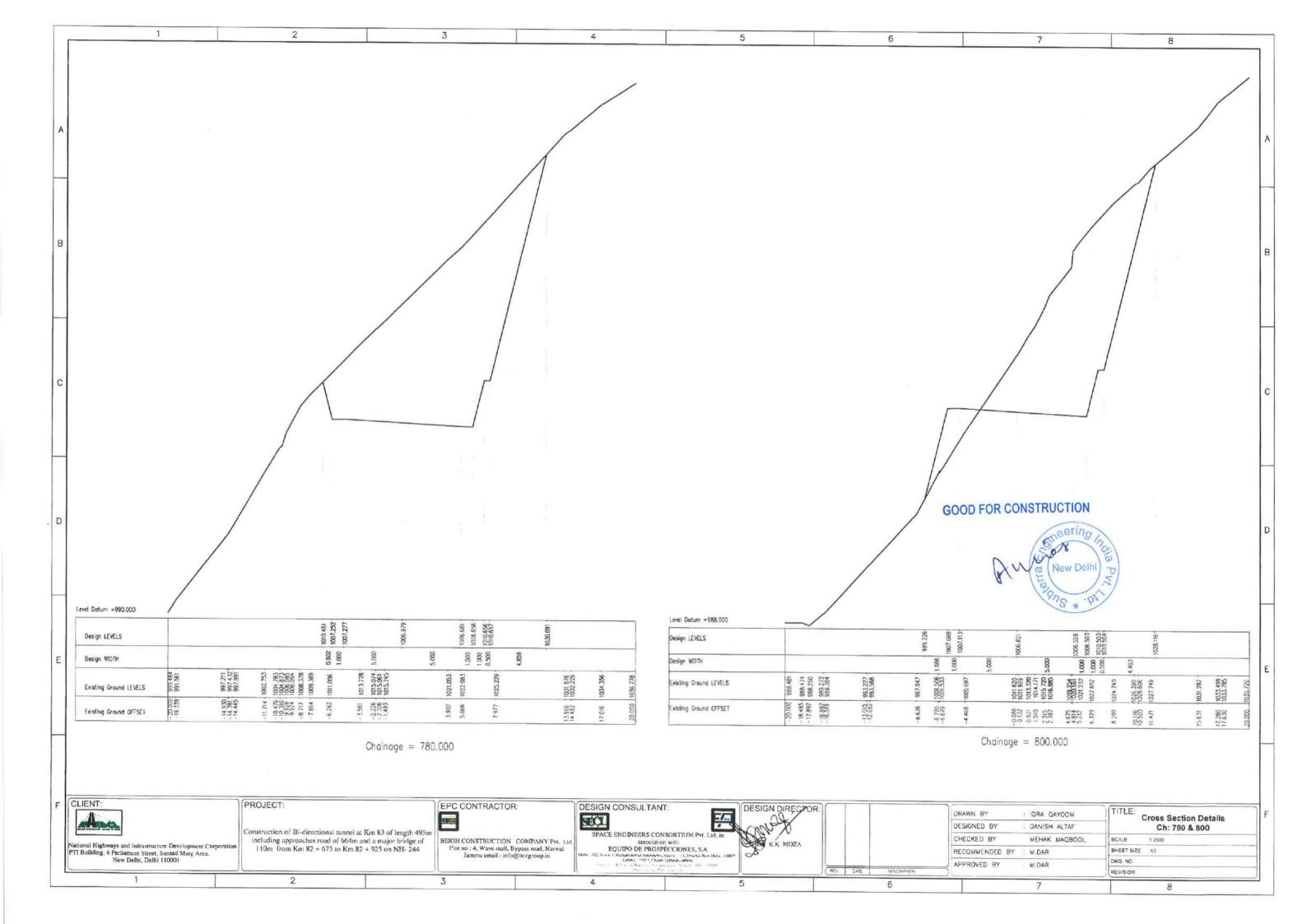


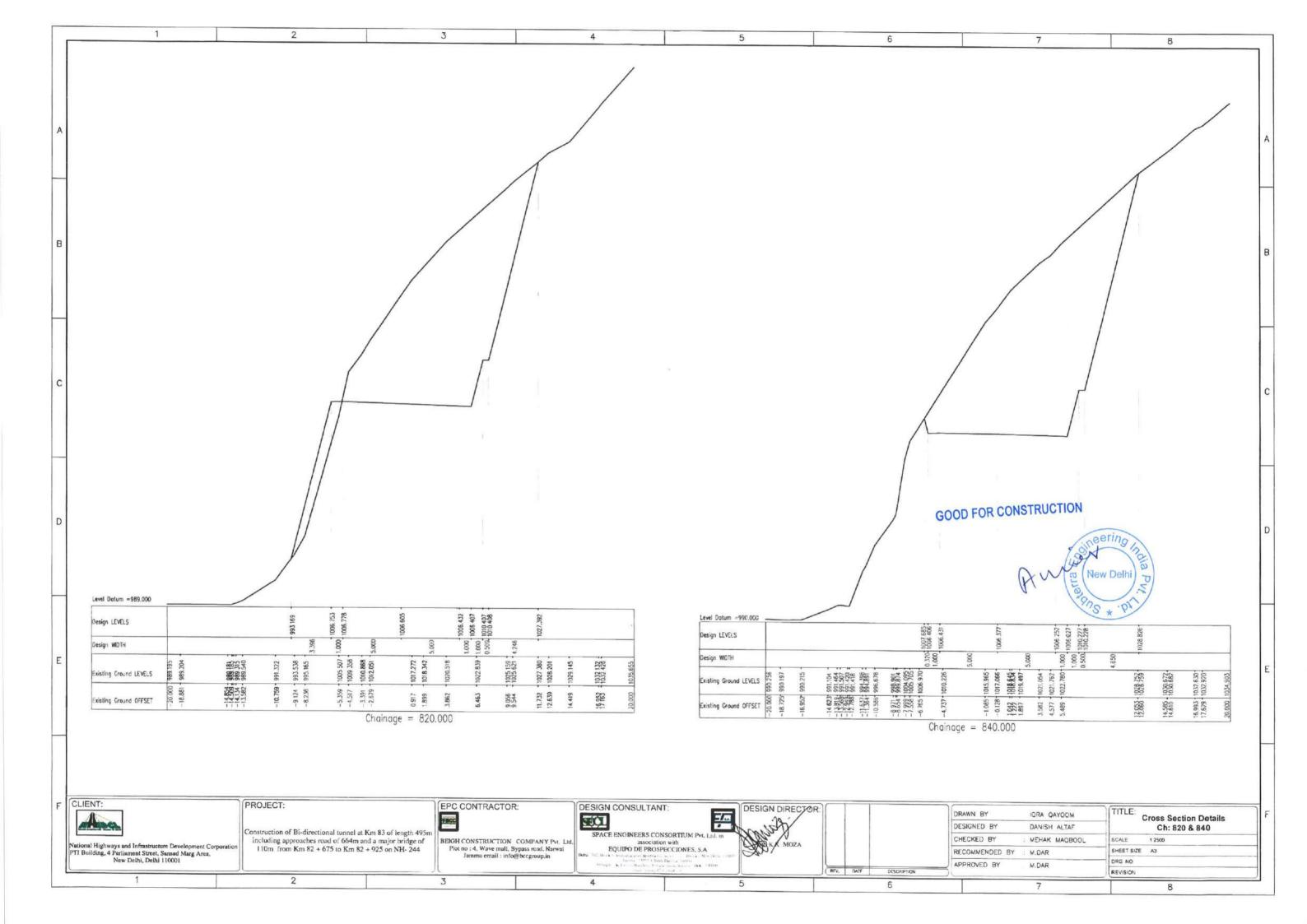


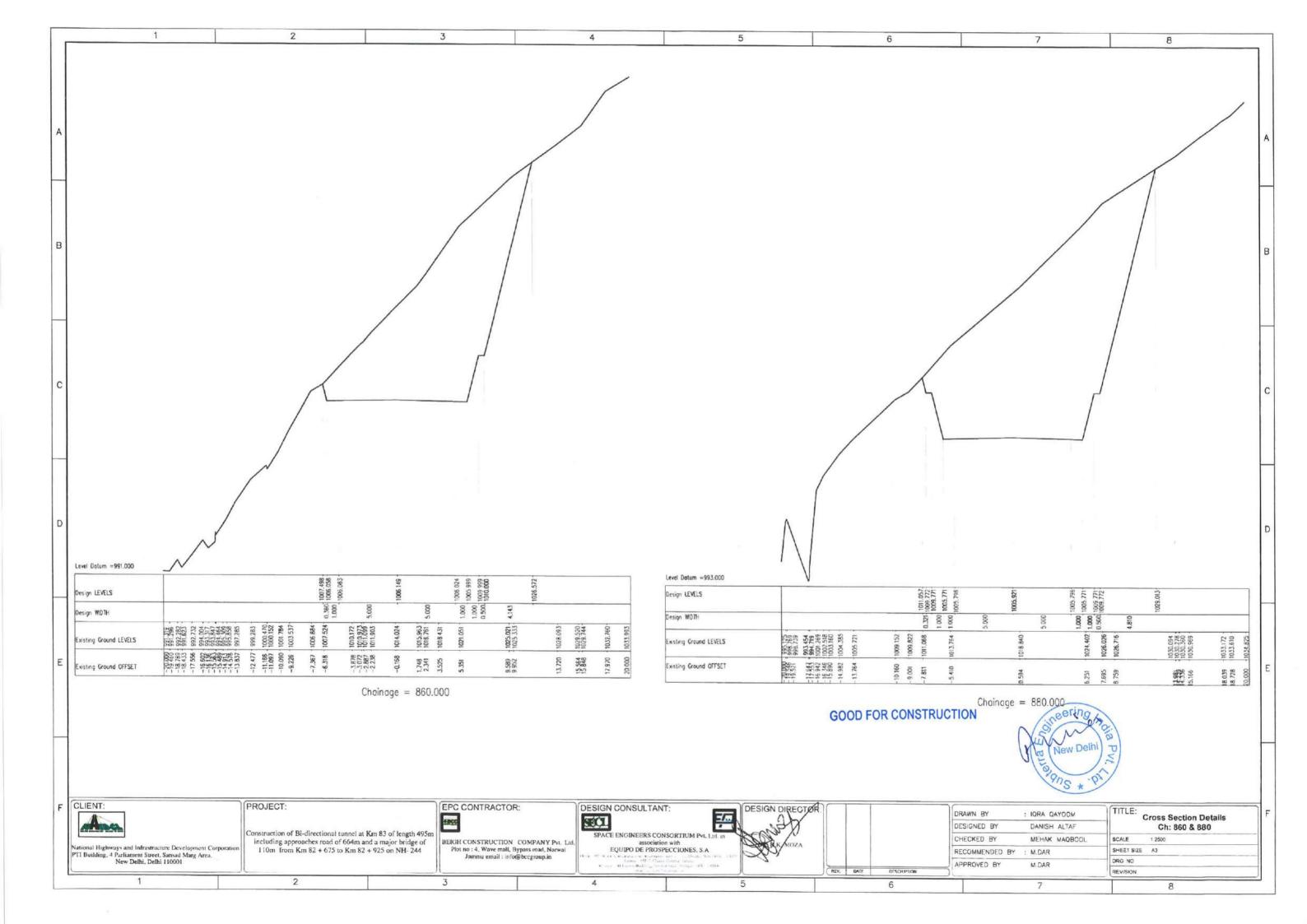


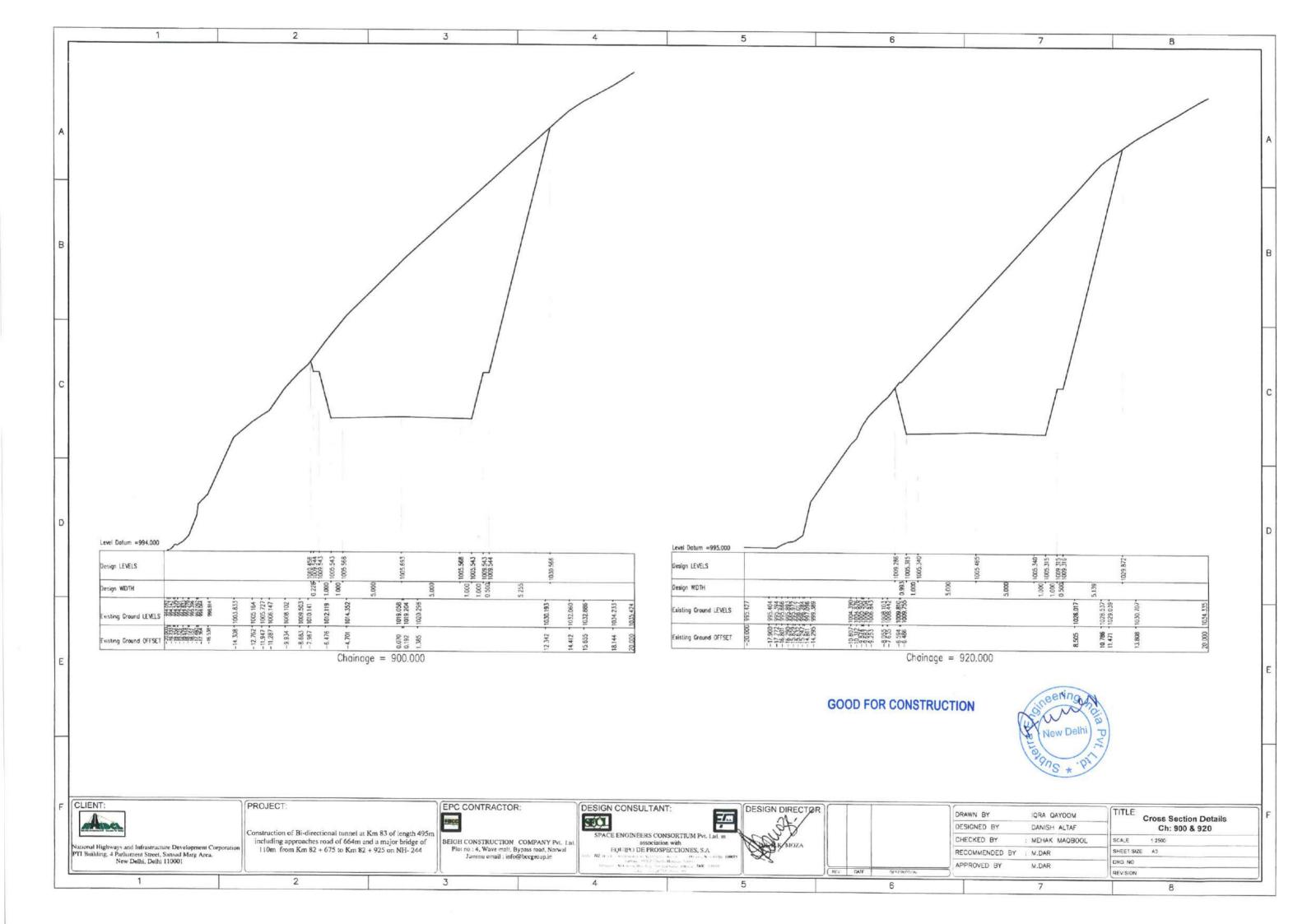


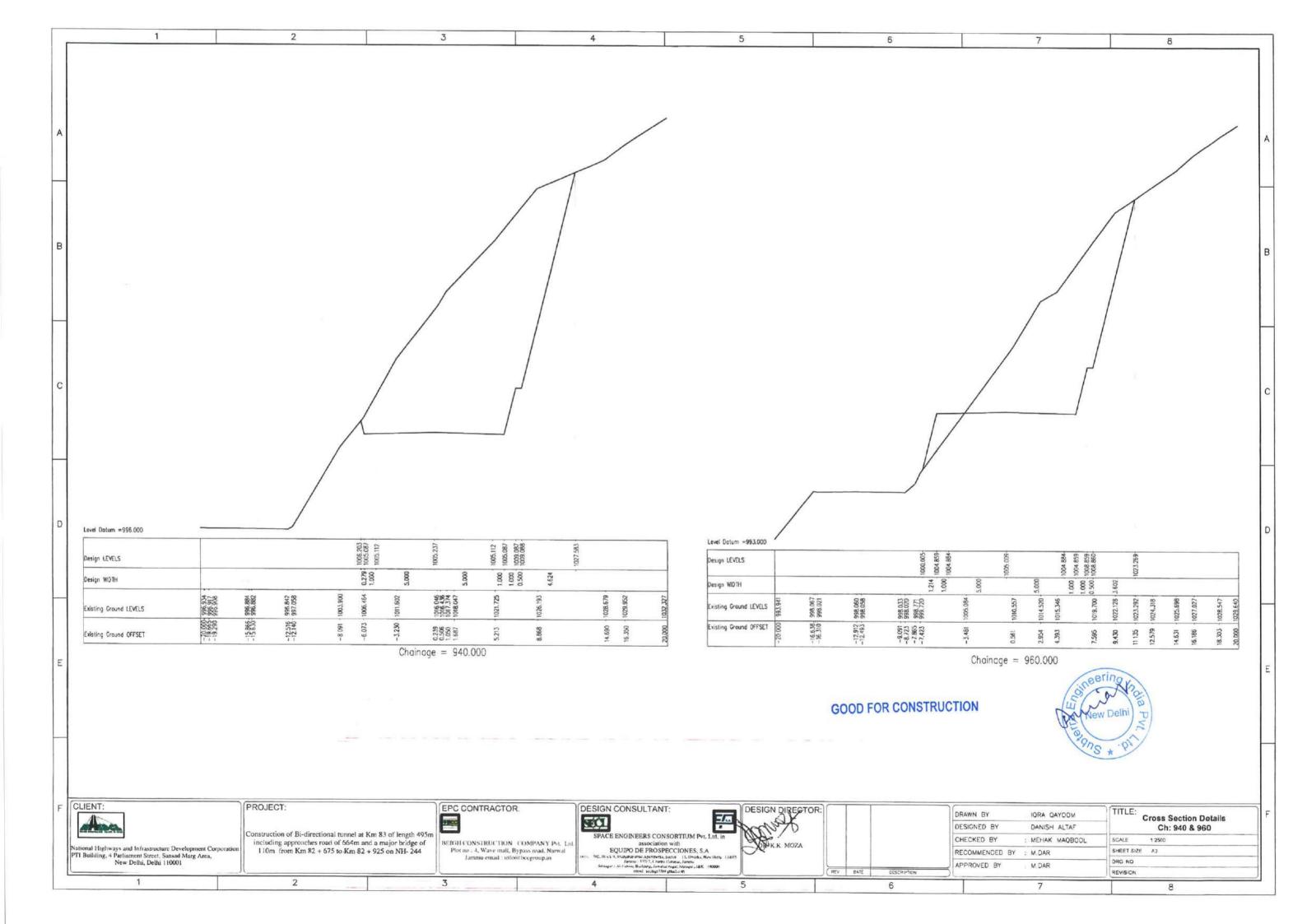


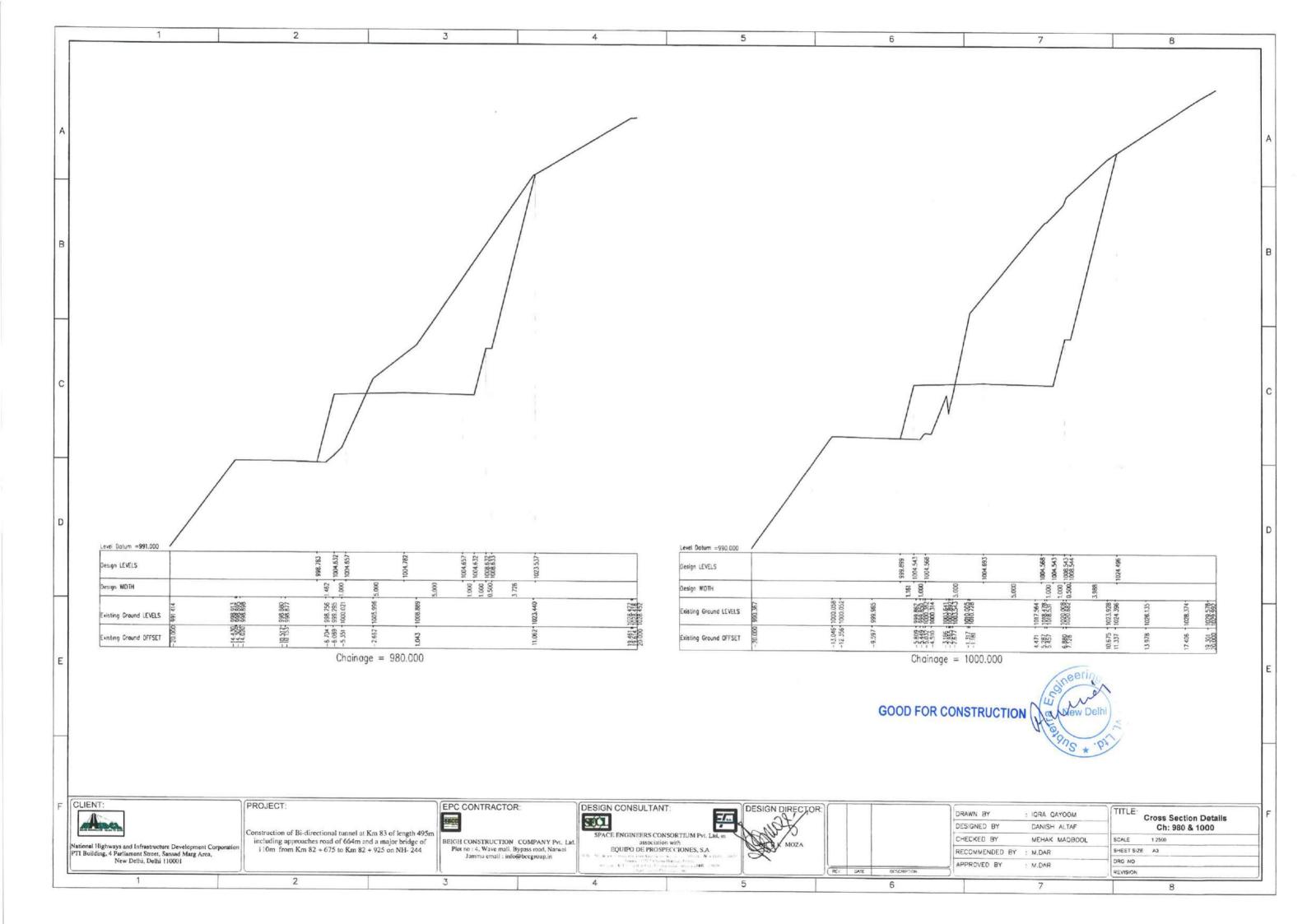


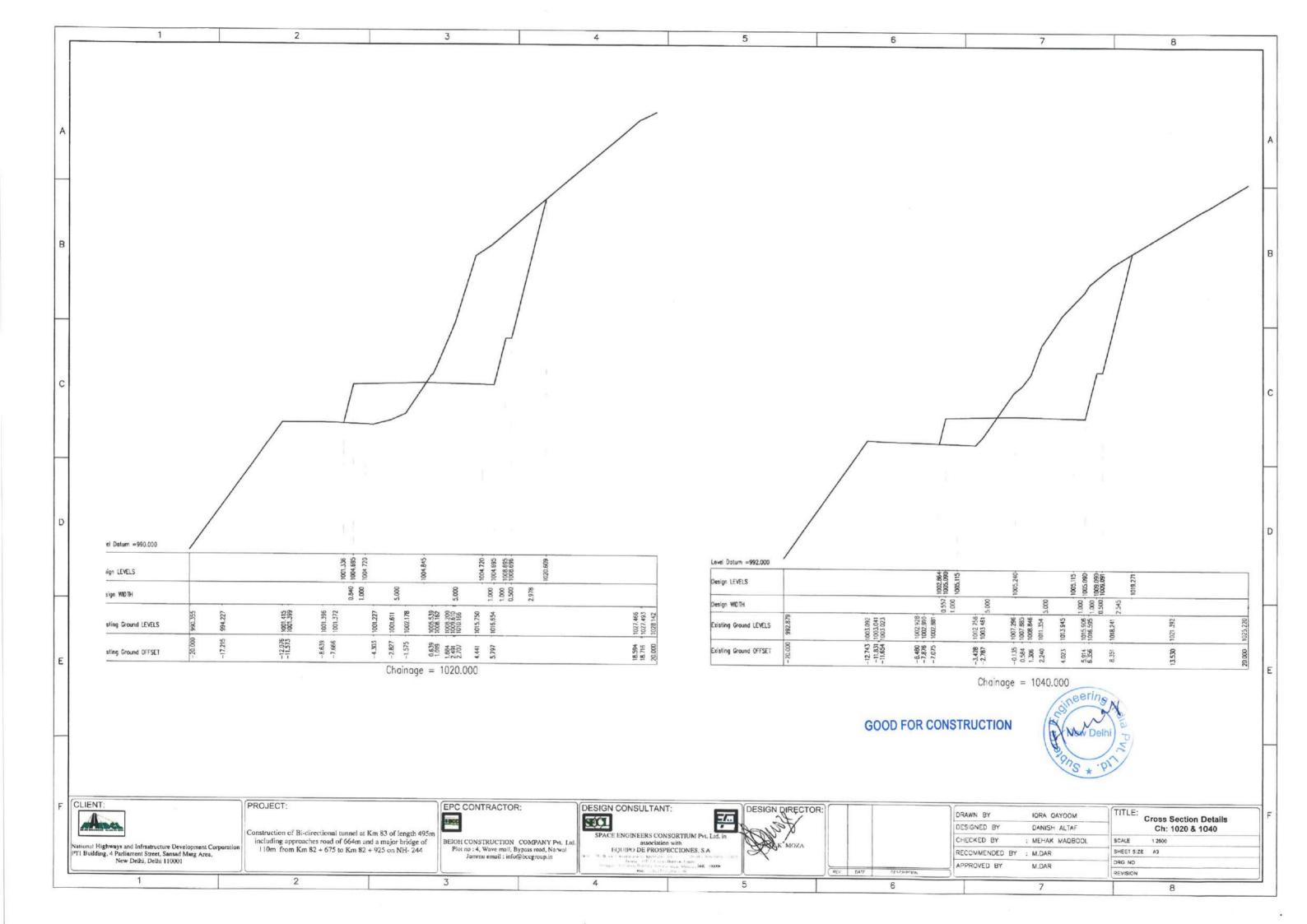


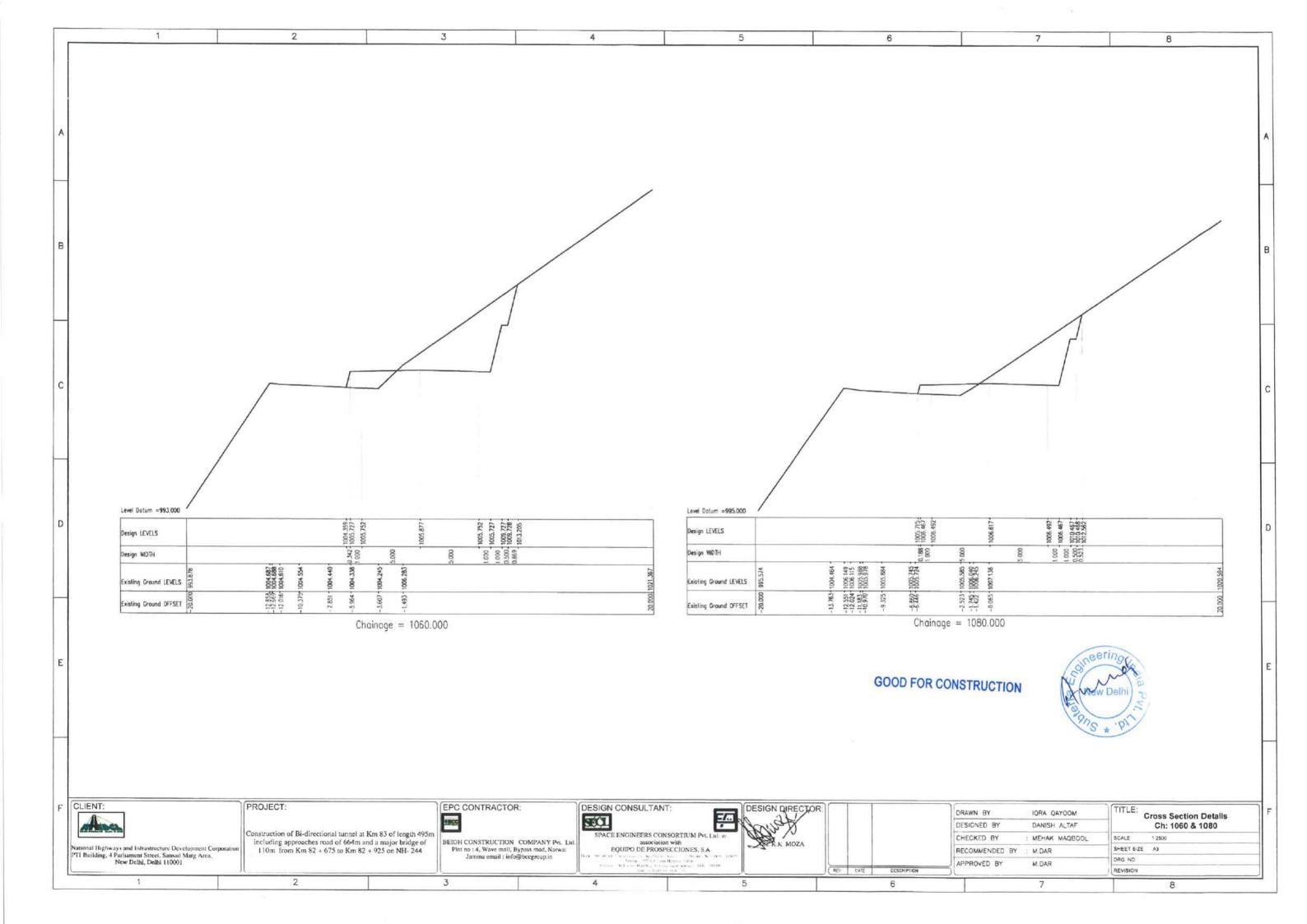


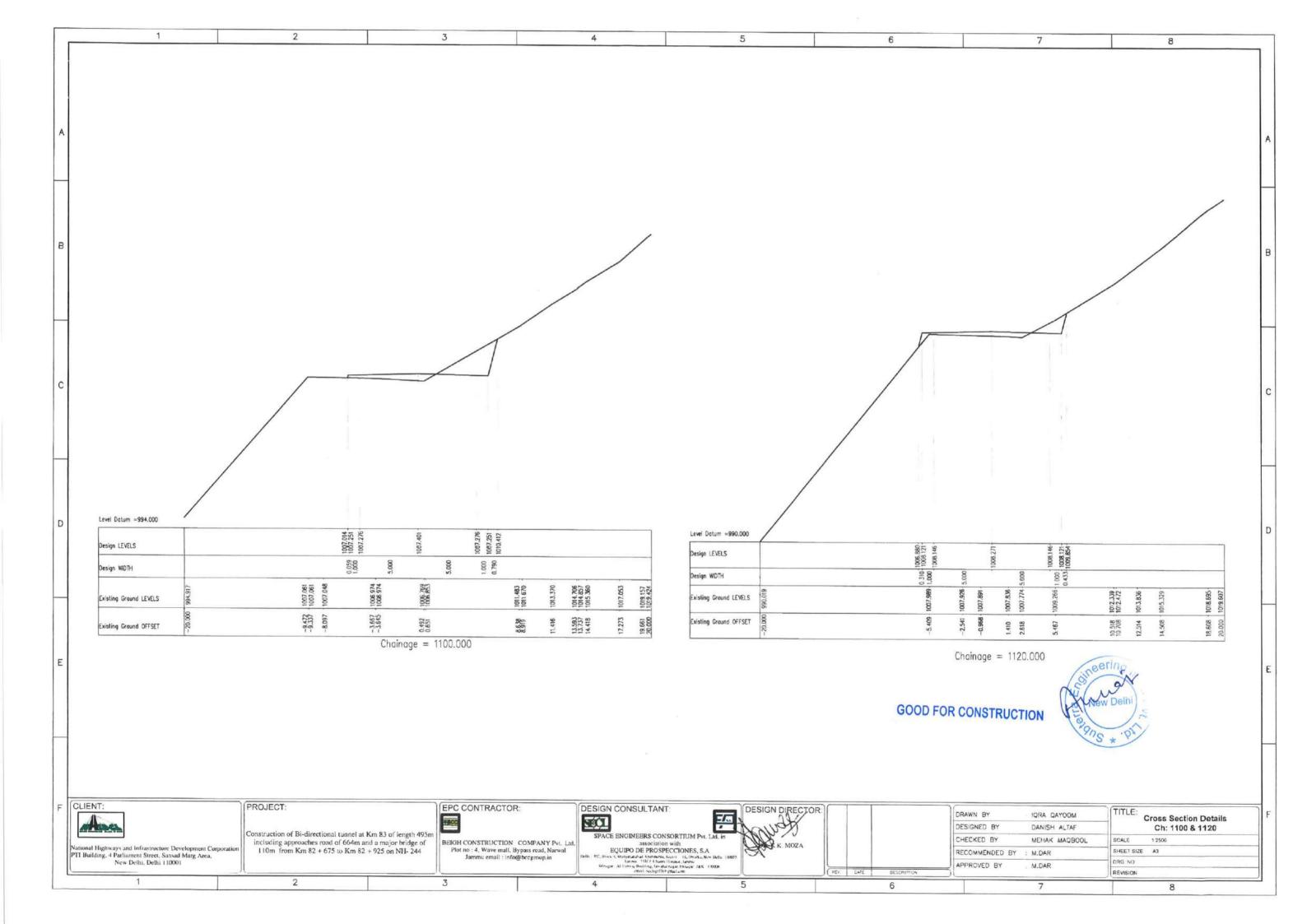


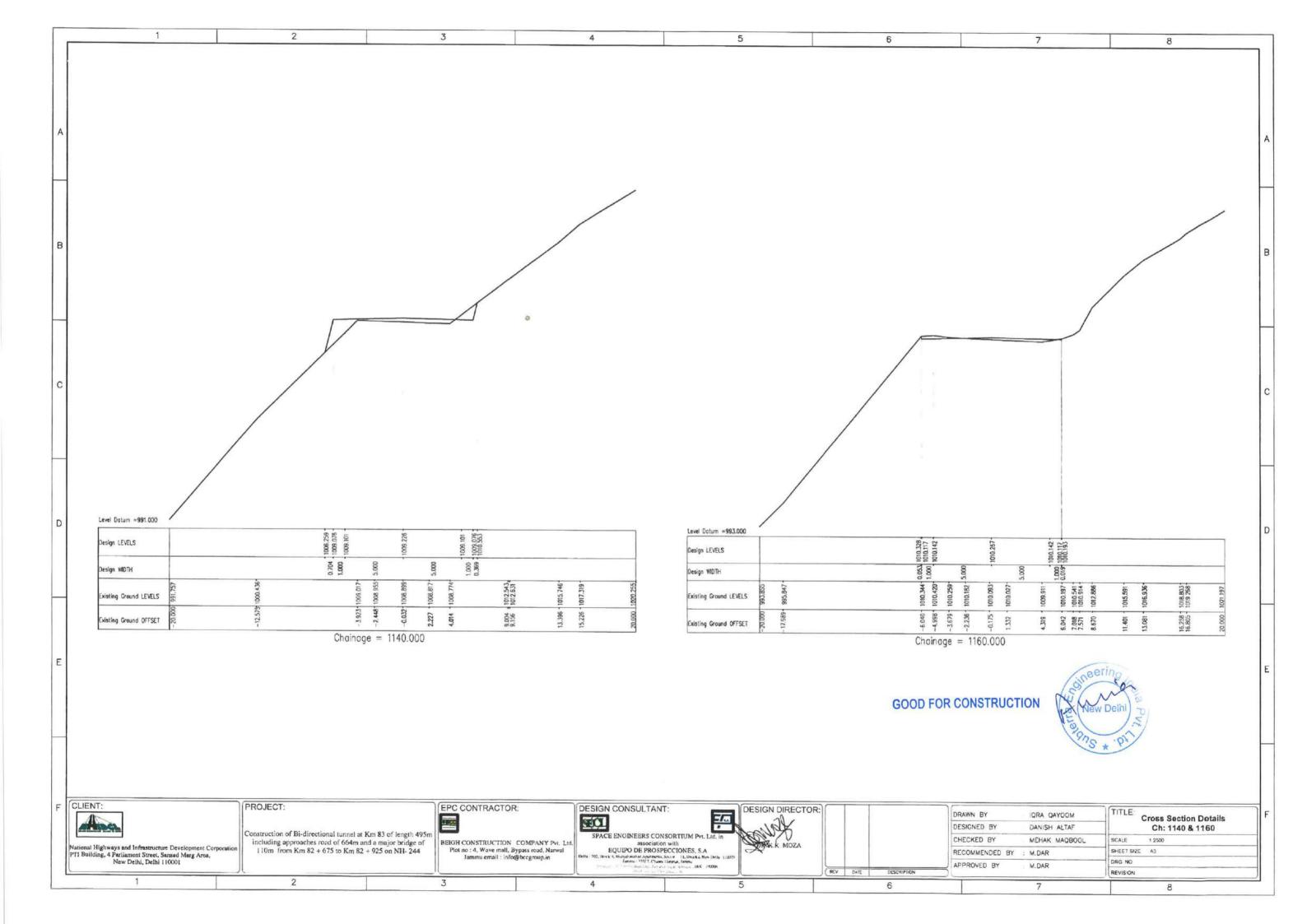


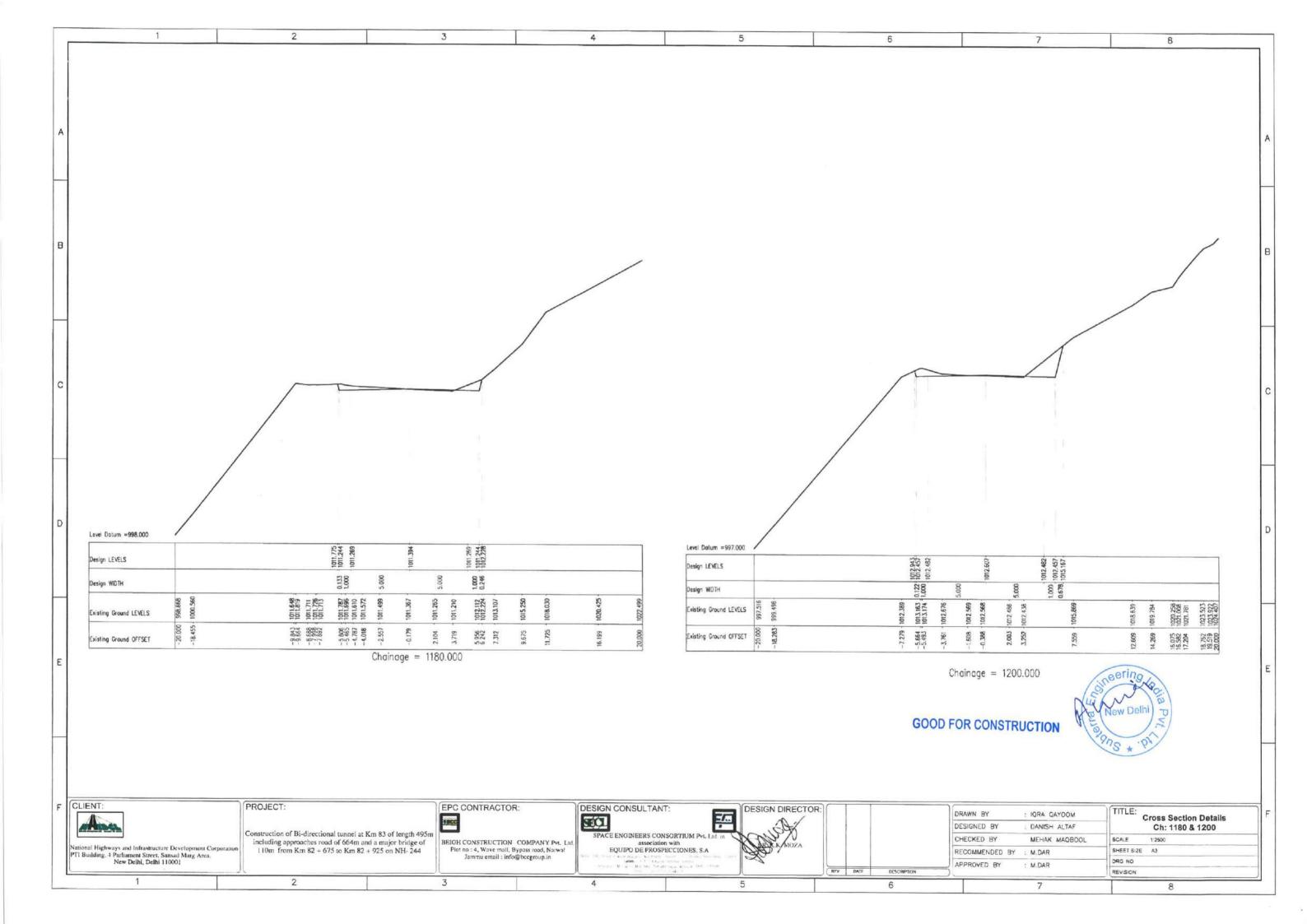


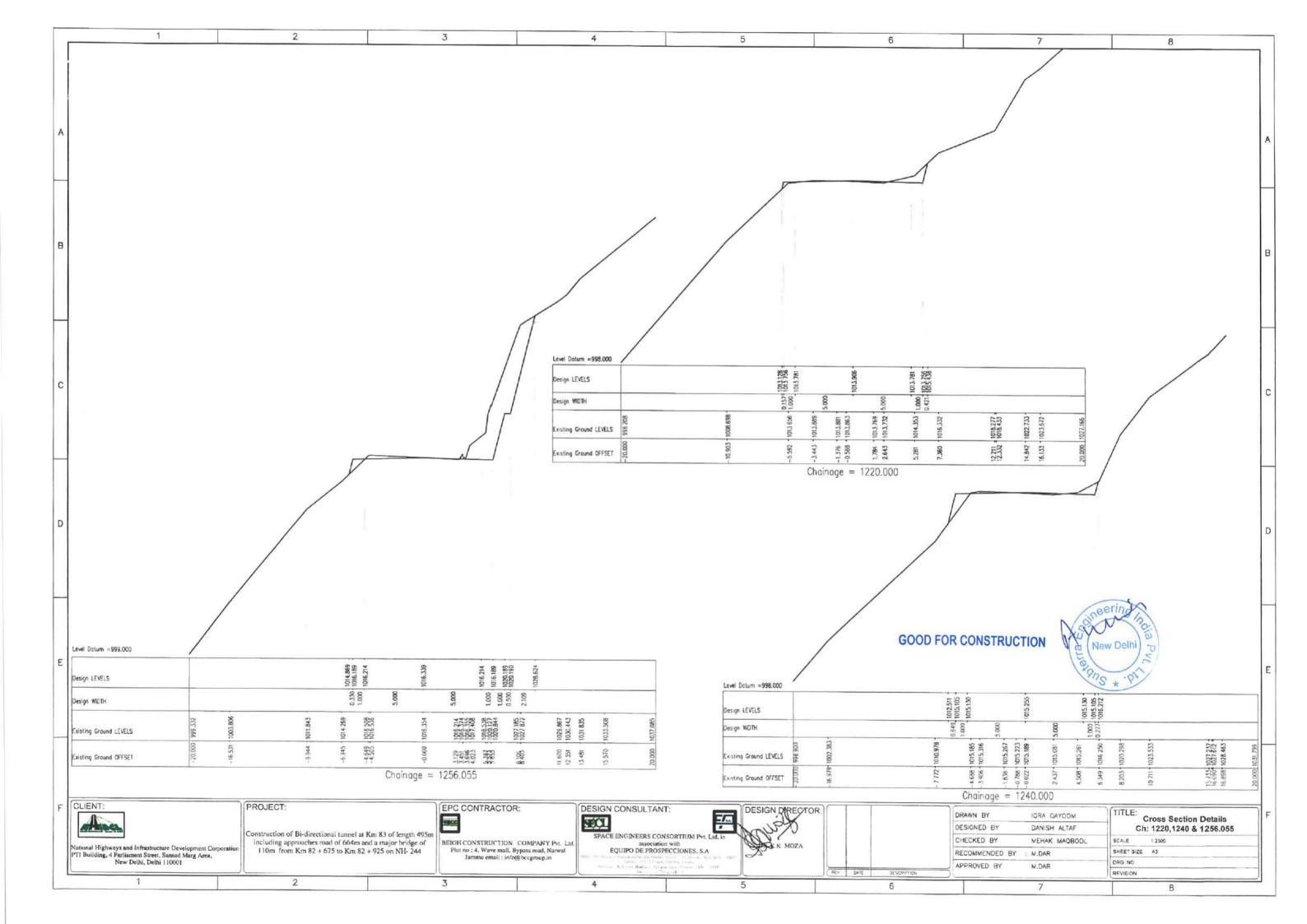


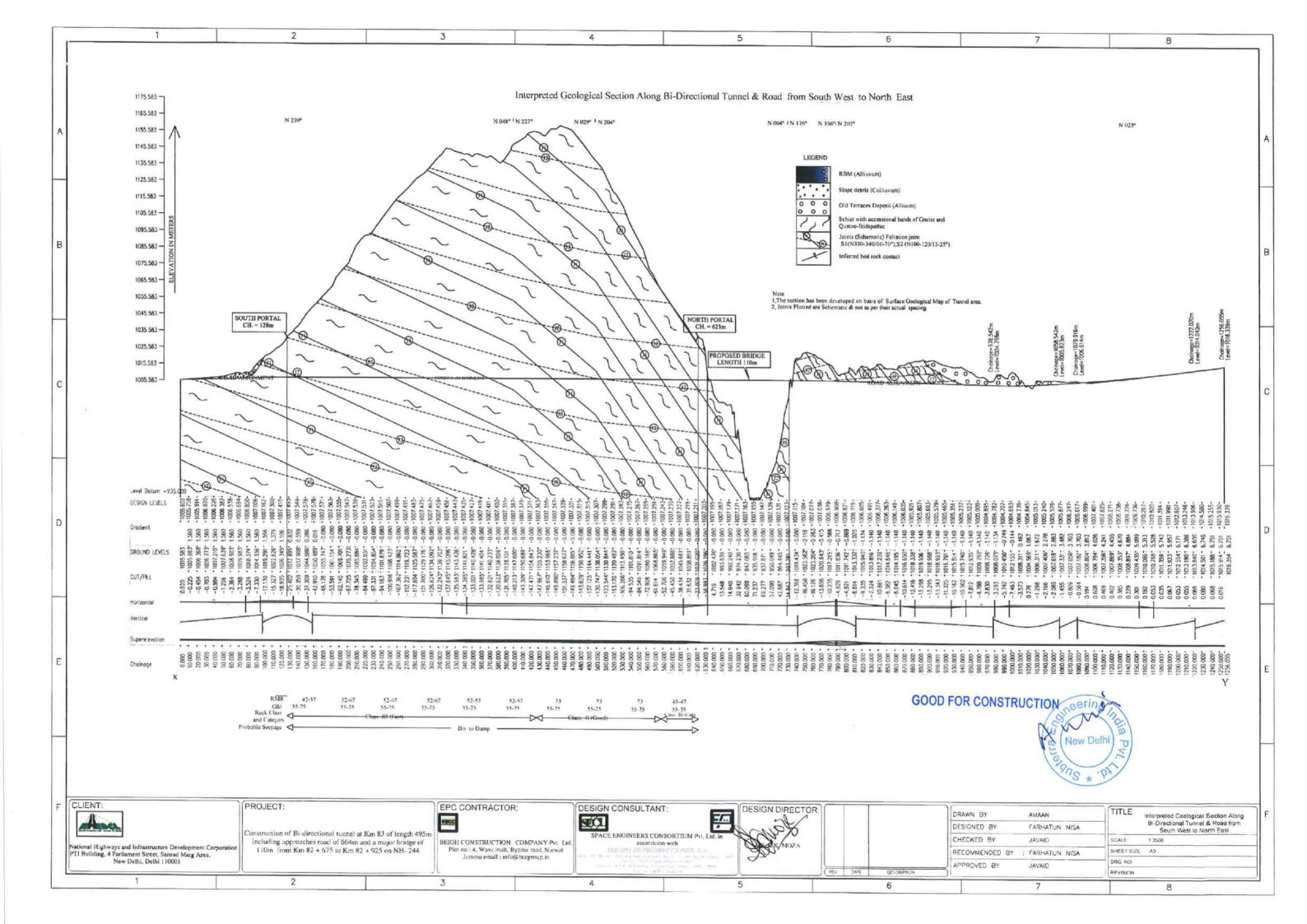


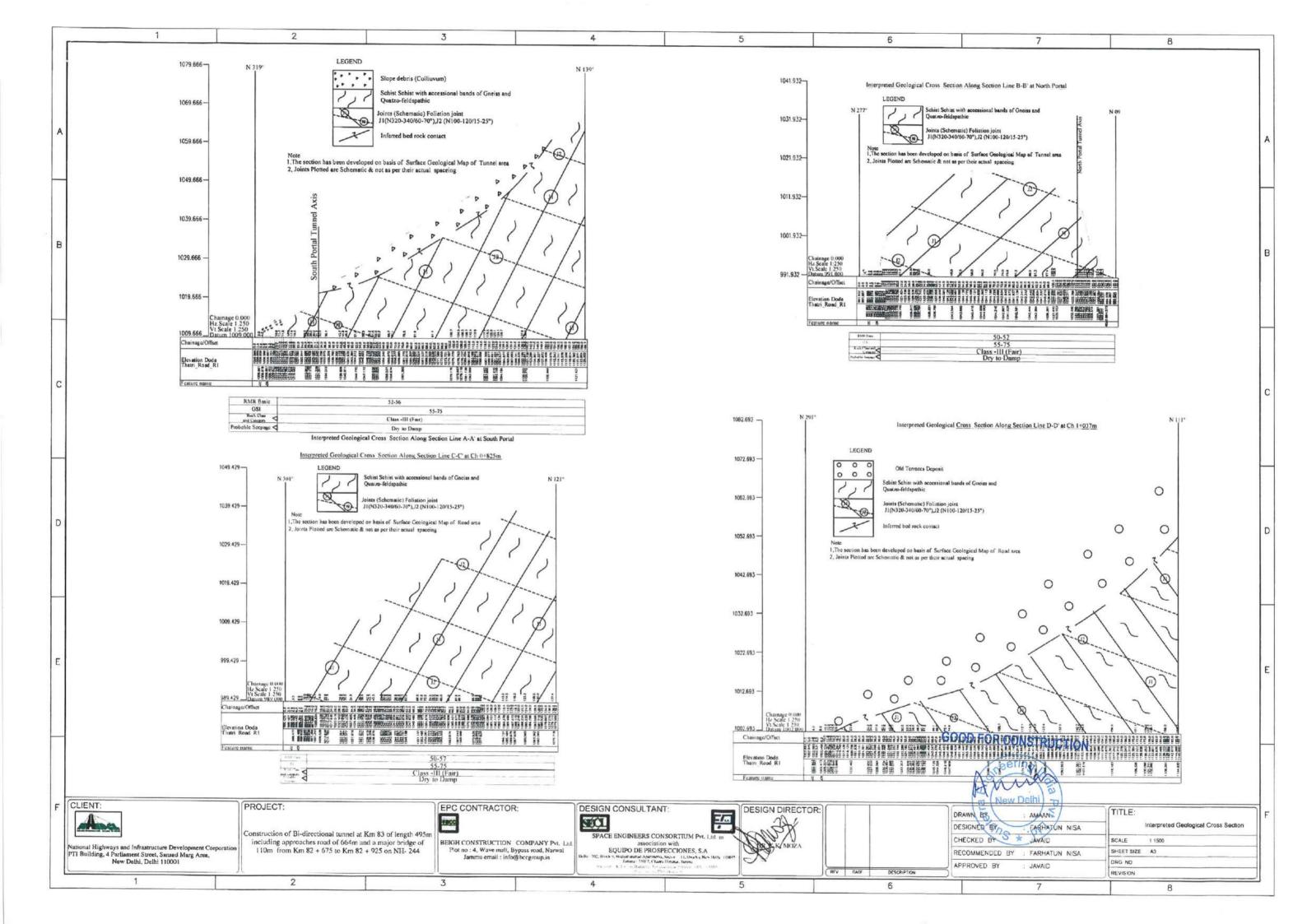


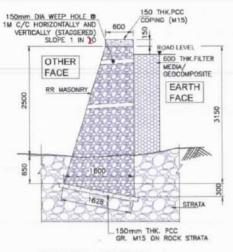




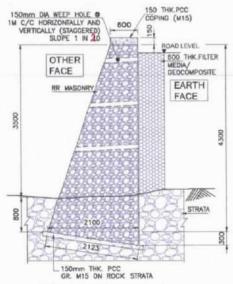




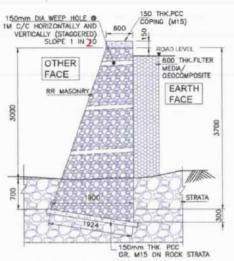




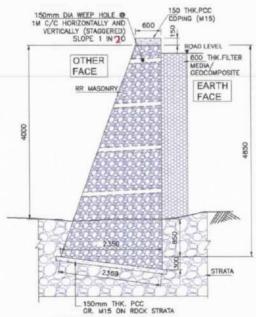
TYPICAL SECTION - 1 FOR RR, DRY MASONRY RETAINING WALL OF HEIGHT 2.5M



TYPICAL SECTION - 3
FOR RR. DRY MASONRY RETAINING
WALL OF HEIGHT 3.5M



TYPICAL SECTION - 2
FOR RR. DRY MASONRY RETAINING
WALL OF HEIGHT 3.0M



TYPICAL SECTION - 4
FOR RR. DRY MASONRY RETAINING
WALL OF HEIGHT 4.0M

## NOTES:-

- ALL DIMENSION ARE IN MILLIMETERS, LEVELS IN METRES
   AND CHAINAGES IN KLONIETERS UNLESS OTHERWISE MENTIONED
- THE DRAWING SHALL BE READ IN CONJUNCTION WITH RELEVANT APPROVED HIGHWAYS PRAWINGS FOR STRUCTURE ORIENTATION, SKEW ANDLE, FRI, & CAMBER/SUPERFLEVATION, ETC.
- 3. 150 DIA WEEP HOLES WITH SLOPE 1 IN 20 SHALL BE PROVIDED AT SPACING OF 1000 CC BOTH HORIZONTALT AND VERTICALLY (STAGGERED) IN FULL HEIGHT OF THE RETAINING WALL WITH BOTTOM MOST ROW 150MM ABOVE GL.
- 4. BACK FILLING AND GEO COMPOSITE MEMBRANE BEHIND THE RETAINING WALL SHALL CONFIRMING TO IRC/78-2014 HAVING PROPERTIES @ 38 (C=0. CONTRACTOR WILL ENSURE CAREFUL PLACEMENT OF BACKFILL AND PROPER PACKING, PROPER BONDING OF MASONRY COURSES AS PER SPECIFICATIONS OF IRC:SP: 48-1988.
- 5. CEMENT MCRTAR (1:3) IS TO BE GIVEN FOR COPING.
- THE REQUIRED SAFE BEARING CAPACITY IS 20 T/SQM, WHICH SHOULD BE CHECKED AND VERIFIED AT SITE BEFORE EXECUTION OF WORK, IF ANY VARIATION NOTICED, IT SHOULD BE INFORMED TO THE DESIGN CONSULTANT.
- 7 MINIMUM EDGE AT TOE END SHALL BE MINIMUM 900MM FROM TOE AS PER IS 1904

## RR. MASONRY SPECIFICATIONS (AS PER IS 1597(1):1992)

- 1 SIZE: THE LENGTH OF STONE SHALL NOT EXCEED THREE TIMES THE HEIGHT ANDEREADTH ON BASE SHALL NOT BE GREATER THAN THREE FOURTH OF THICKNESS OF WALL NOR LESS THAN 1500mm, THE HEIGHT OF STONE FOR RUBBLE MASONRY MAY BE UP TO 300mm.
- 2 MATERIAL: ALL STONES USED SHALL BE OF STRONG HARD AND DURABLE. ALSO IF SHOULD BE FREE FROM DEFECTS LIKE CAVITIES CRACKS FLAWS, SAND HOLES, THE PERCENTAGE OF WATER ABSORPTION NOT EXCEED 8 PERCENT.
- 3 CONSTRUCTION OPERATIONS: THE STONE SHALL BE LAID SO THAT THE PRESSURE IS ALWAYS PERPENDICULAR TO THE NATURAL BED. STONES SHALL BE SUFFICIENTLY WETTED BEFORE LAYING TO PREVENT ABSORPTION OF WATER FROM MORTARVERTICAL JOINTS SHALL BE STAGGERED AS FAR AS POSSIBLE, BELL SHAPED BOND STONES AS HEADERS SHALL NOT BE USED.

  AT ALL ANGULAR JUNCTIONS THE STONES AT EACH ALTERNATE COURSE SHALL BE WELL BONDED INTO RESPECTIVE COURSES OF THE ADJACENT WALL.





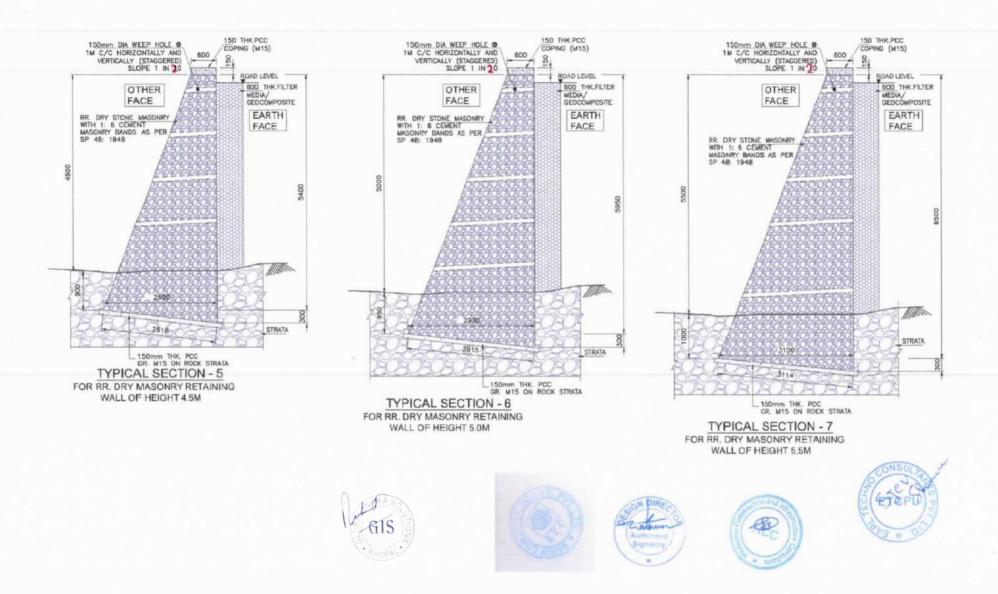


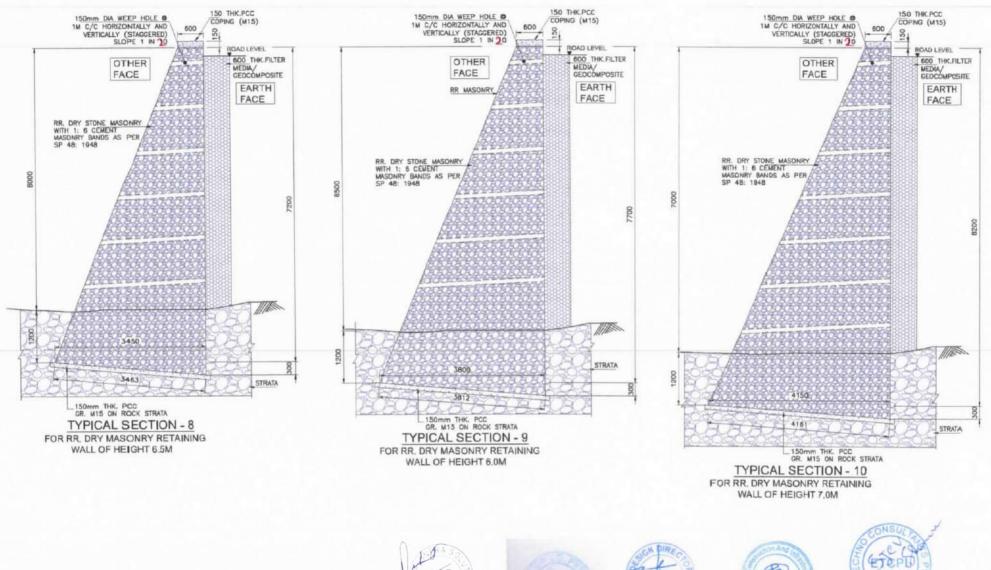




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